

The TUCAN next generation UCN source

overview and some details

R. Picker

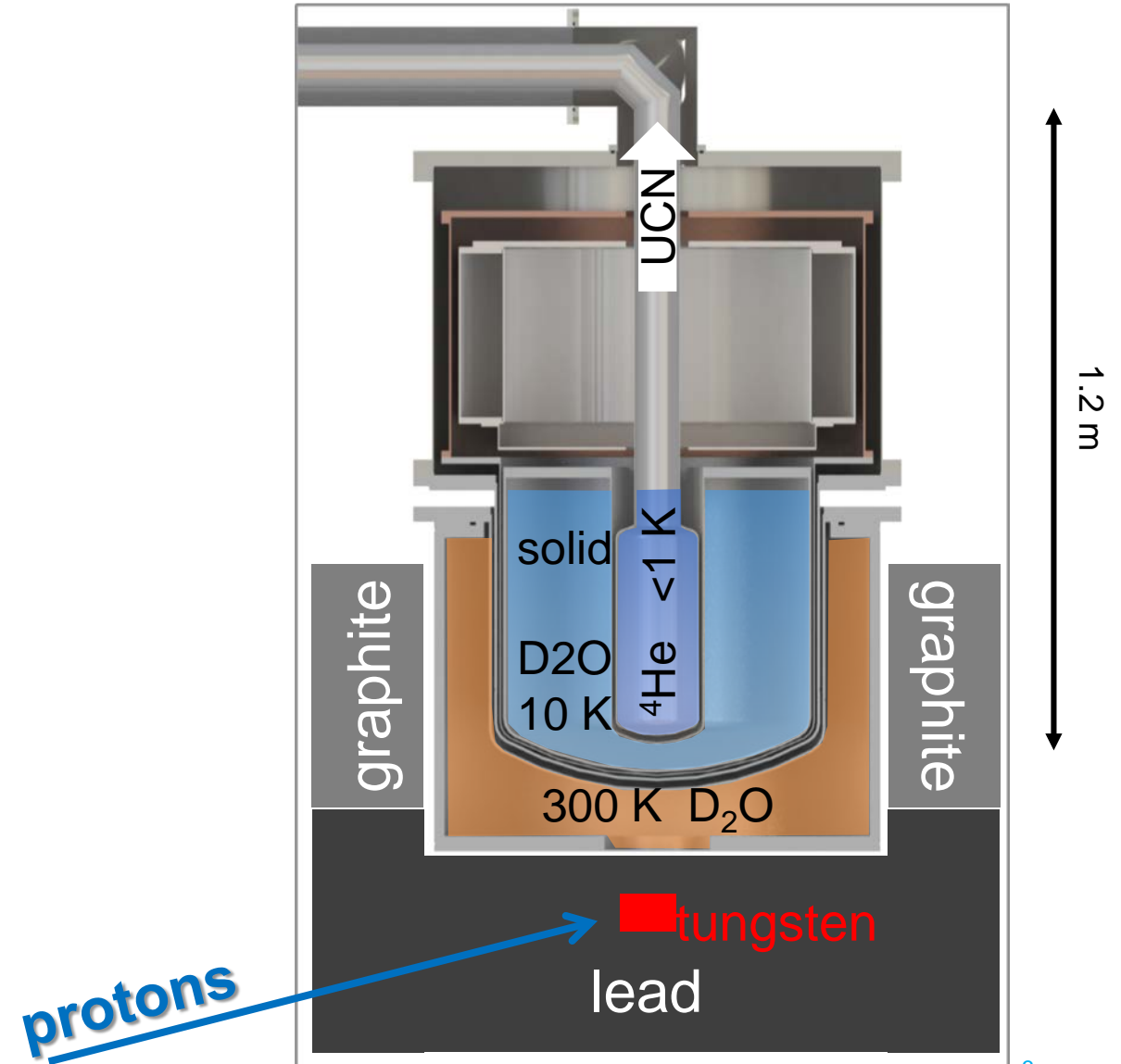


C. Davis, B. Franke, C. Gibson, K. Hatanaka,
T. Higuchi, S. Horn, S. Kawasaki, S. Imajo, T. Kikawa,
A. Konaka, F. Kuchler, T. Lindner, Y. Makida,
R. Mammei, C. Marshall, J.W. Martin, R. Matsumiya,
K. Mishima, T. Okamura, R. Picker, D. Rompen,
W. Schreyer, S. Sidhu, S. Vanbergen

- UCN source key numbers
- Source components and model
- Schedule
- Monte Carlo Optimization of UCN components
- Gas handling systems, pumps and transfer line

using the prototype source as example

1. 480 MeV protons on tungsten create **spallation neutrons**
2. lead, graphite, heavy water, (deuterium) **moderate** fast neutrons (MeV) to cold neutrons (meV)
3. ^4He at around 1 K **converts** 1 meV (9\AA) neutrons **to UCN**
4. **Extraction** to experiments via material guides



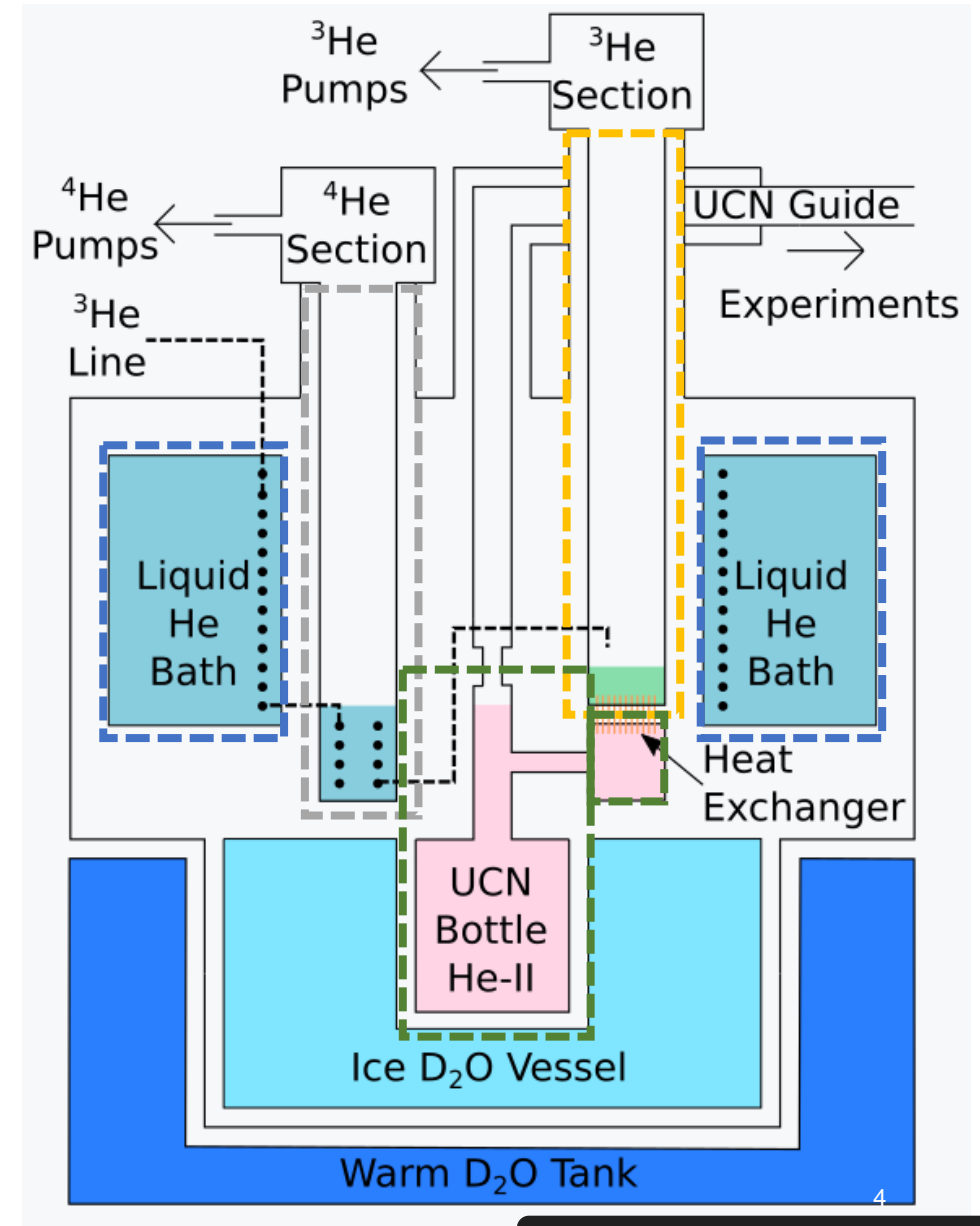
from KEK/RCNP, Japan

3 cooling stages, heat exchanger to cool isopure ^4He UCN converter

- ^3He bath cryostat (4.2 K)
- ^4He pumping section (1.6 K)
- ^3He pumping section (< 1.0 K)
- Isopure ^4He UCN converter cooled via heat exchanger

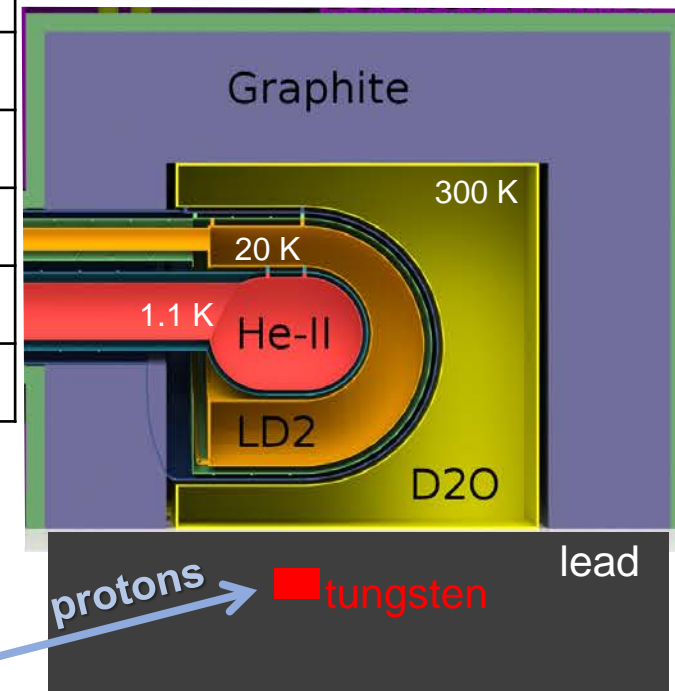
⇒ Running nominally at 1 μA beam (as at RCNP).

W. Schreyer, tomorrow



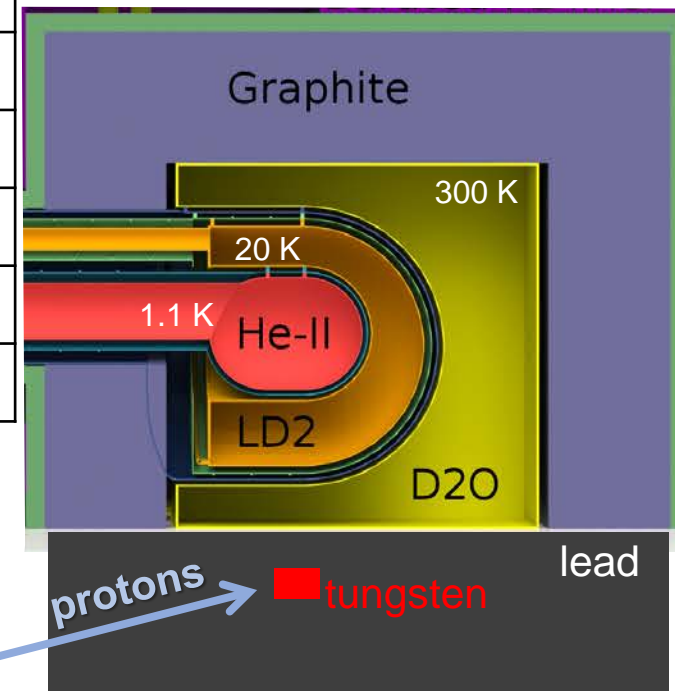
Similar basic layout with major improvements:

Parameter	Prototype source	Next gen source
Beam current	1 μA	40 μA (480 MeV)
Production volume	8 L	27 L
Cold moderator	sD ₂ O	LD ₂
Production rate	$2 \times 10^5 / \text{s}$	$1.4\text{-}1.6 \times 10^7 / \text{s}$ ($500 \text{ s}^{-1} \text{cm}^{-3}$)

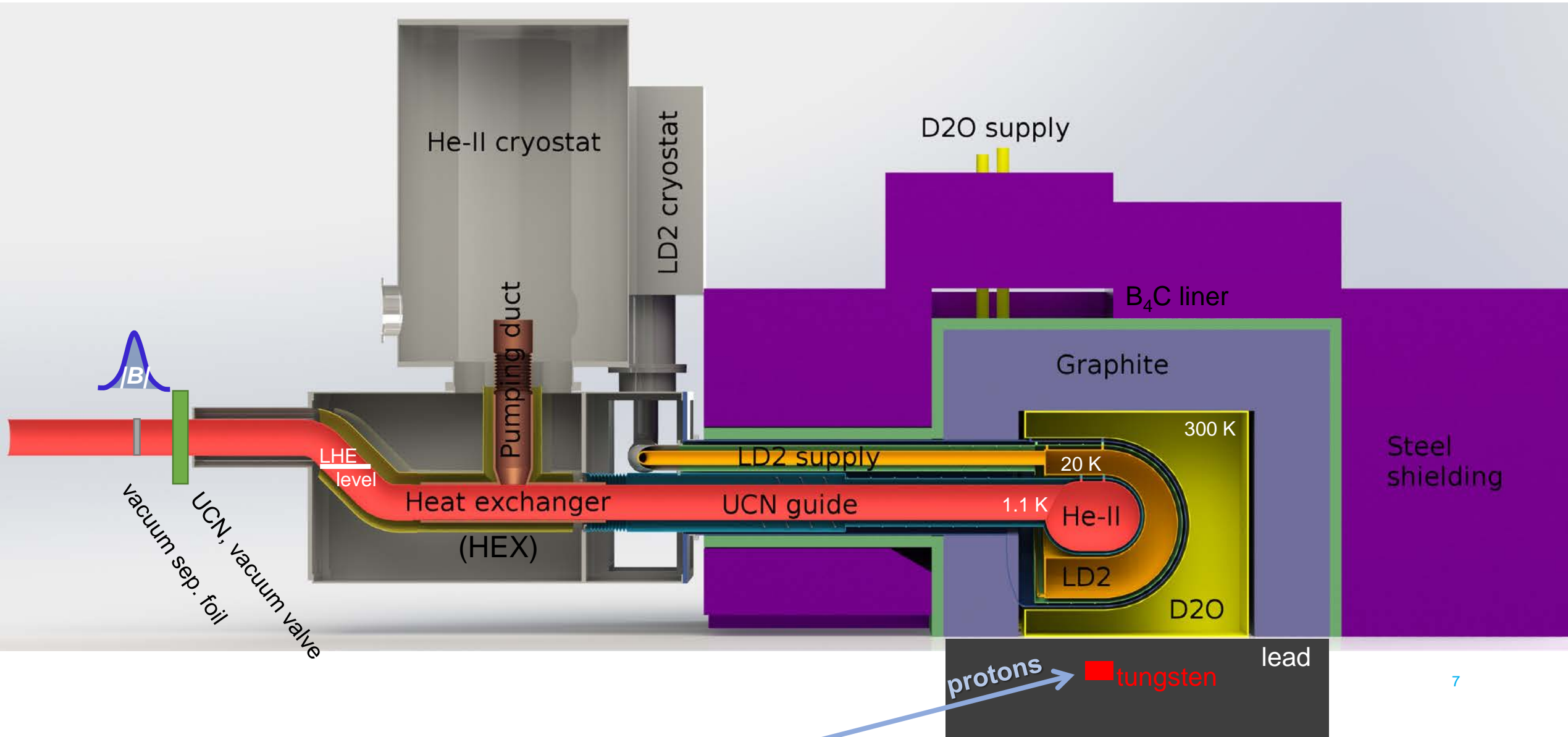


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Production volume	8 L	27 L
Cold moderator	sD ₂ O	LD ₂
Production rate	$2 \times 10^5 / \text{s}$	$1.4 - 1.6 \times 10^7 / \text{s}$ ($500 \text{ s}^{-1} \text{cm}^{-3}$)
Cooling power	0.3 W	10 W
He-II temperature	0.9 K	1.1 – 1.15 K
Extraction	Vertical by 1.2 m	Near horizontal 0.3 m up
Vacuum separation	No foil	Warm vacuum sep foil + B field
Position of cryostat	On top of source	2.5 m away



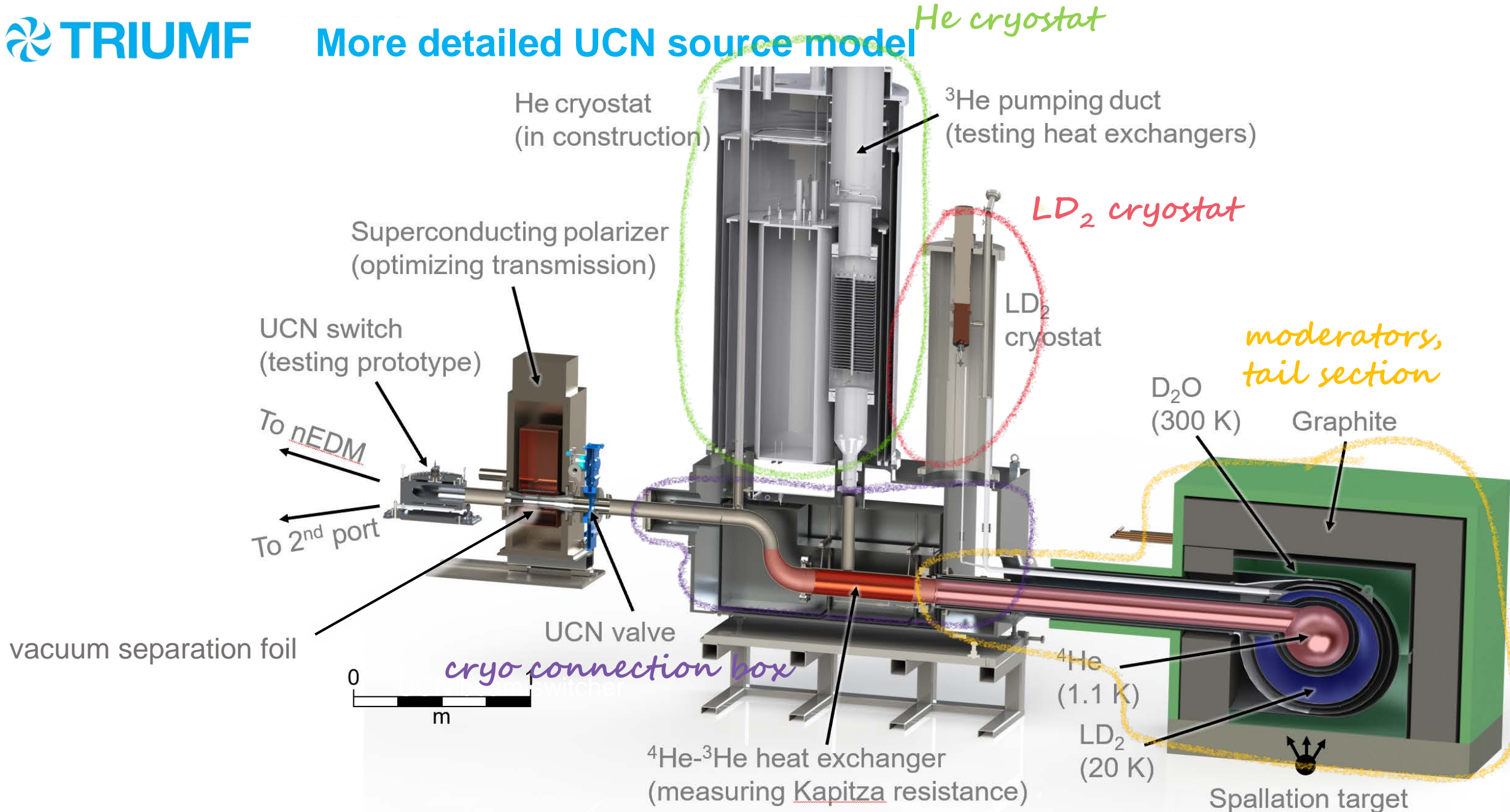
← ≈ 2.5 m →

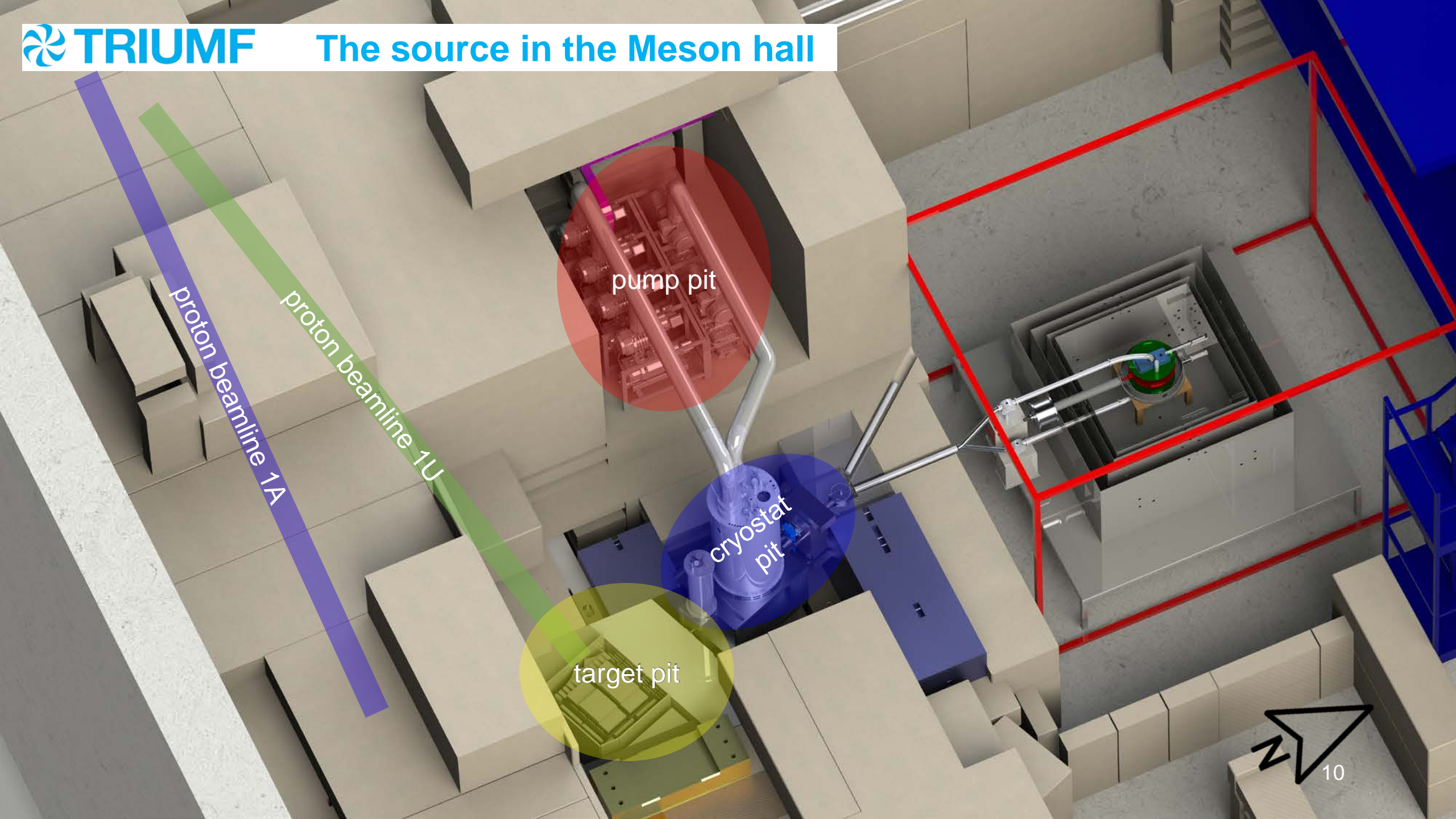


- Large cold flux in UCN production volume \Rightarrow D_2O , LD_2 moderators, graphite reflector C. Marshall W. Schreyer
- Large thermal load from spallation source \Rightarrow lead shield plus geometry optimization W. Schreyer
- **More material, more heat** \Rightarrow **near-spherical shape of UCN production volume** C. Marshall
- Large cooling power below 1 K \Rightarrow pumping on 3He (10000 m³/h \Rightarrow 10 W) S. Kawasaki
- Incompatibility of 3He with UCN \Rightarrow UCN friendly 3He - 4He heat exchanger (flat surface inside) S. Kawasaki
- 3He very expensive \Rightarrow **staged HEX approach and “cheap” 3He ?** S. Kawasaki
- **Kapitza resistance large at 1 K** \Rightarrow **large HEX surface (approx. 0.3 m²)** S. Kawasaki
- Cannot put cryostat right on top of target \Rightarrow UCN guide \equiv heat conduction channel (2.5 m long) S. Kawasaki
- **Low heat conductivity of He-II at 1 K** \Rightarrow **large UCN guide diameter (15 cm)** S. Kawasaki
- Freeze-out on cold vacuum separation foil \Rightarrow warm vacuum separation foil (inside B field) RP
- Containment of liquid helium \Rightarrow (small) vertical rise in liquid filled UCN guide (23 cm) This presentation
- **Limited supply of liquid helium** \Rightarrow **design efficient cryostat** S. Kawasaki, C. Gibson
- **Large amount of deuterium required** \Rightarrow **inherent and/or redundant safety systems (safety approval)** C. Marshall
- **Radiative heat input to SF LHE surface** \Rightarrow **testing UCN friendly radiation heat suppressors** RP, W. Schreyer

<https://doi.org/10.1016/j.nima.2020.163525>

More detailed UCN source model





proton beamline 1A

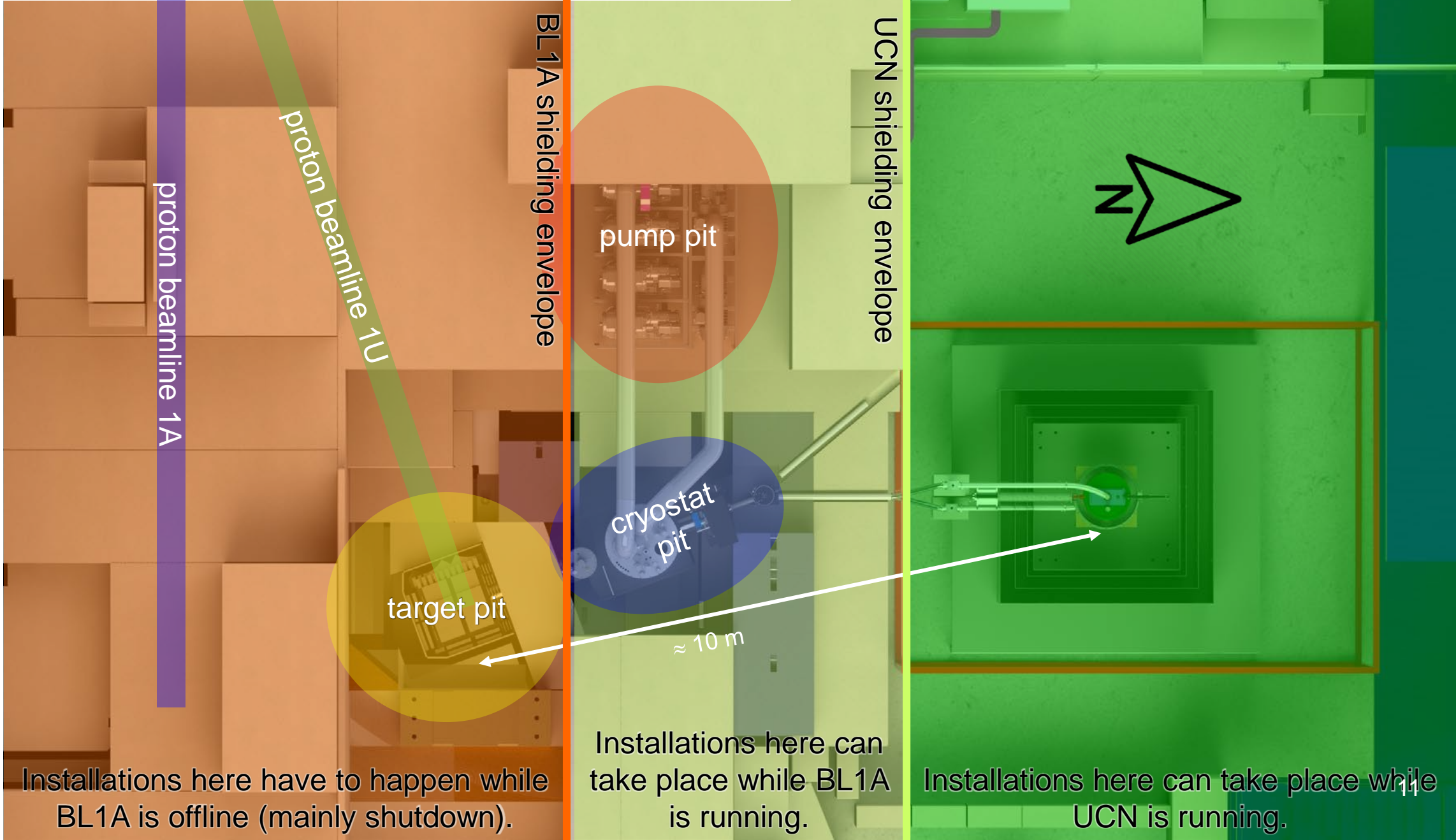
proton beamline 1U

pump pit

cryostat pit

target pit





Installations here have to happen while BL1A is offline (mainly shutdown).

Installations here can take place while BL1A is running.

Installations here can take place while UCN is running.

TUCAN source (engineering stage)

- Production $1.4-1.6 \times 10^7$ UCN/s
- Source helium temp 1.03 K to 1.13 K
- Cooling power 10 W (3He fridge)
- Source storage lifetime 28 s
- Figure of merit $P\tau = 4.5 \times 10^8$
- Density in the source 3×10^3 UCN/cc
- Total number in the source 3×10^8 UCN
- Initial polarized density in 70 l EDM experiment 200 UCN/cc (> 10 m of guide)
- Counted at the end of cycle 2×10^6

Summer 2018

- **JSPS** (Japan Society for the Promotion of Science) **funding** for the helium cryostat has been granted at 152 MJPY.
- Final decision to go for **³He cryostat** (not ⁴He direct pumping).
- Initial System Engineering Design (System Block Diagram, Top level Requirements, nEDM Experiment Requirements, He Cryostat Requirements, LD₂ Subsystem Requirements, Initial Spec Sheets generation)
- **Preliminary LD2 Safety Report** Released
- Initial release of UCN yield versus moderator and source design report
- Released designs for UCN experiments in Fall 2018
- Released **schematics** (P&IDs) for He-II Subsystem, LD2 Subsystem
- Released initial **design concept for biological shielding**

Fall 2018

- **Tested first components for the new UCN source** during 1-month of UCN beamtime at TRIUMF (UCN friendly vent port, UCN source valve, superconducting polarizer)
- Performed UCN storage tests with a mock-up UCN production volume (NiP coating on aluminum) and determined that a bake out temperature of 100 C is sufficient.
- Liquid deuterium system conceptual design received positive concept review from the safety authority Technical Safety BC.
- Additional **requirements documents** released: He-II Subsystem, Simultaneous Spin Analyzer Subsystem
- Some **cryogenic calculations** completed for He-Cryostat and LD2 Subsystem

Winter 2019

- Additional requirements documents released: remaining source subsystems, nEDM Cell, UCN Guidance
- Initial **3D concept of LD₂** Subsystem
- Initial stress calculations and 3D Model for the multi-layered source vessel containing LD₂ and superfluid helium
- Early orders for D2O

Spring 2019

- Finished the bulk of UCN and **cryogenics related calculations** necessary to start detailed design.
- Measurements at KEK confirm the **Kapitza conductance** at the 3He to 4He heat exchanger is in good agreement with our models.
- Additional requirements documents released: Internal magnetometry
- TRIUMF **design review of biological shielding** passed.
- TRIUMF **design review of He cryostat pumping** system passed
- Positive initial discussions with Technical Safety BC about LD2 system safety
- **Hemispherical production volume and moderator geometry chosen**

Summer 2019

- Target protect monitor (TPM) of BL1U commissioned
- **Detailed design of helium cryostat** completed, start of production in Japan.
- Confirm **superleak tightness** of a new designed **helicoflex seal** flange at KEK (it will be used for junction of the HEX1, which is the main heat exchanger, and the UCN guides.
- Confirm superleak tightness of a **junction of aluminum and stainless** steel at KEK (it will be used for UCN guide upstream of the helium cryostat)
- **HEX7 test** successfully completed at KEK (counterflow gas heat exchanger from room temperature to 10 K)

Fall 2019

- **UCN source storage valve** upgrade tested successfully during UCN beamtime.
- **TRIUMF design review of He cryostat** passed.
- Important interfaces between He cryostat and remainder of He-II subsystem confirmed
- **UCN Y switch** completed

Winter 2020

- **HEX5 test** successfully completed at KEK (counterflow gas heat exchanger in the 1K pot pumping tube)



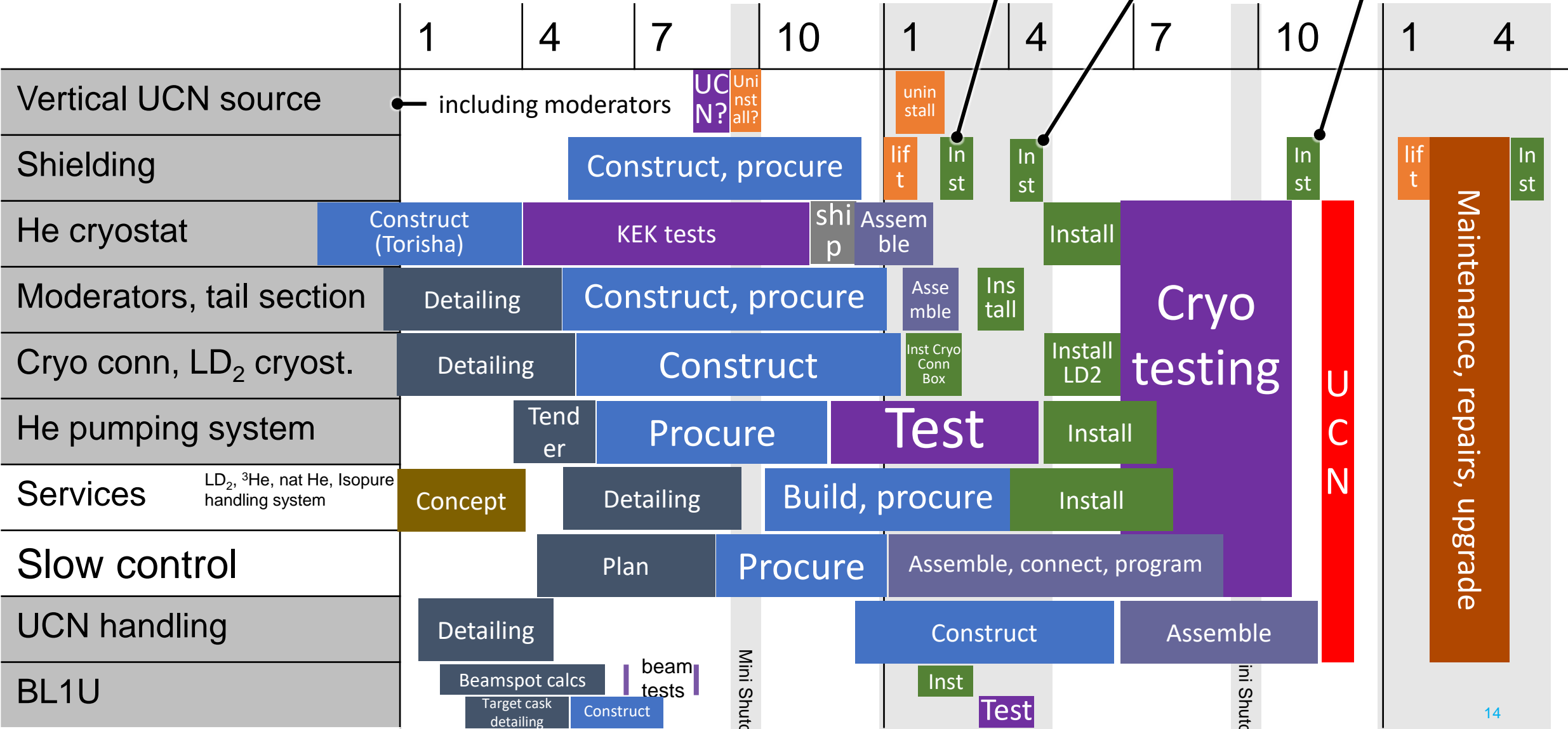
UCN source schedule

Calendar Year

2020

2021

2022



prepare moderator region

to allow BL1 operation

to allow BL1U operation

UCN

Maintenance, repairs, upgrade

Gray shaded systems are inside the biological shielding.

Mini Shutdown

Main Shutdown

Mini Shutdown

Main Shutdown

General remarks

- He cryostat components are tested pre-assembly at KEK (2019/2020)
- Extensive cryo testing of all components planned for 2021
- He cryostat can be cooled down without cooling LD₂ system
- Currently developing a more detailed installation and testing plan

Planned test campaigns

LD₂

- LD₂ handling system test with N₂
- LD₂ cryostat cooldown

He cryostat

- Cryo testing at KEK (no ³He)
- 1K pot pumping
- ³He pot pumping, probably with ⁴He first
- HEX1 only test (if possible)
- Connect tail section
- Connect downstream UCN guide

Goal: minimize the measurement time to reach a sensitivity $d_n \leq 10^{-27} \text{ ecm}$

Starting point

- Well known **statistical sensitivity formula**

$$\sigma(d_n) \approx \frac{\hbar}{2\alpha T_{\text{Ramsey}} E \sqrt{N_{\text{det}}}}$$

- Naively one thinks you can only improve N_{det} by improving the geometry using UCN MC simulations...
- ... but the energy spectrum also influences the optimal T_{Ramsey} and more...

Steps:

- Perform three separate MC simulations (relevant durations)
 - Simulate filling of EDM cells from UCN source ($T_{\text{accumulate}}$ and T_{fill})
 - Simulate storage in EDM cells (T_{Ramsey})
 - Simulate emptying of EDM cells to detectors (T_{count})
- Calculate $\sigma(d_n)$ for one cycle
Inputs: T1, T2, detector efficiency etc
- Calculate number of cycles needed for $d_n \leq 10^{-27} \text{ ecm}$
- Calculate required calendar days
Inputs: a certain up time per day (≈ 16 hr), degaussing time, E field reversal etc
- Then vary the four durations above to minimize the measurement time. (differential evolution algorithm from the SciPy library)

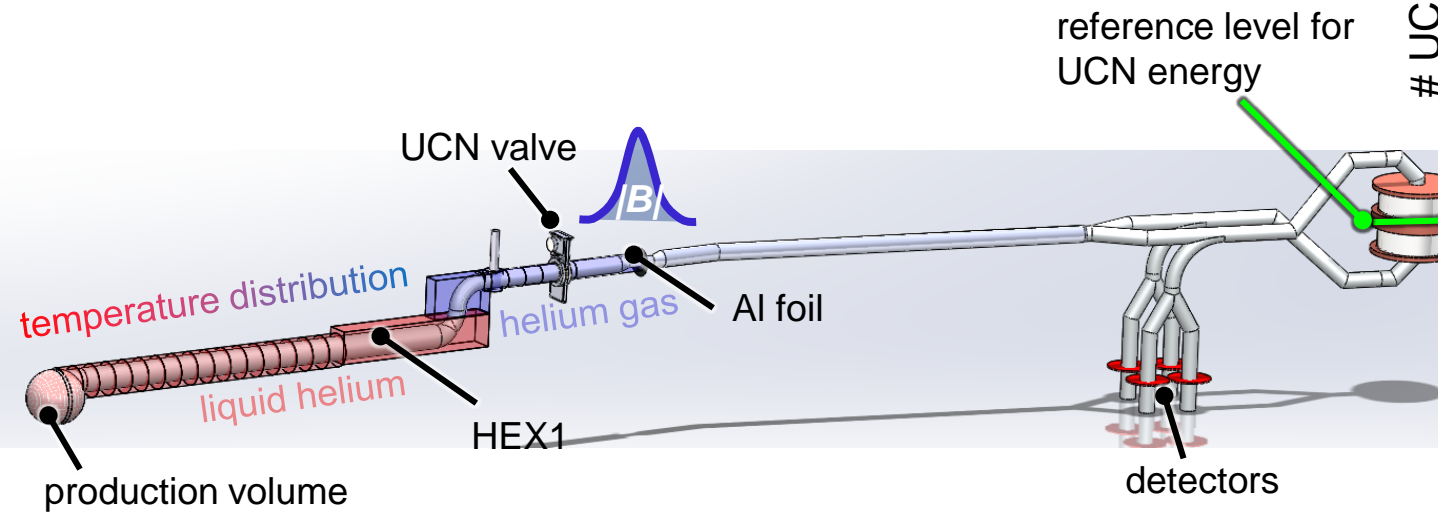
next slides

α visibility \propto polarization

T_{Ramsey} free spin precession time

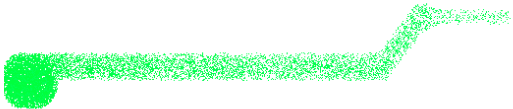
E electric field

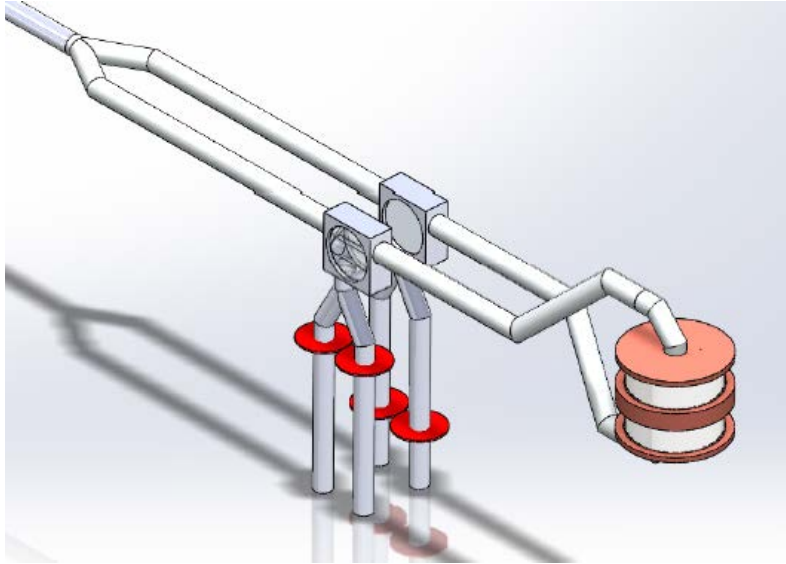
N_{det} # of UCN detected



1. Spawn UCN inside production volume at constant rate with UCN valve closed (Maxwellian tail spectrum)
 $T_{accumulate}$
2. Open UCN valve to start EDM cell filling, keep spawning UCN T_{fill}
3. Record UCN energy distribution in EDM cell every second

Color: UCN production time





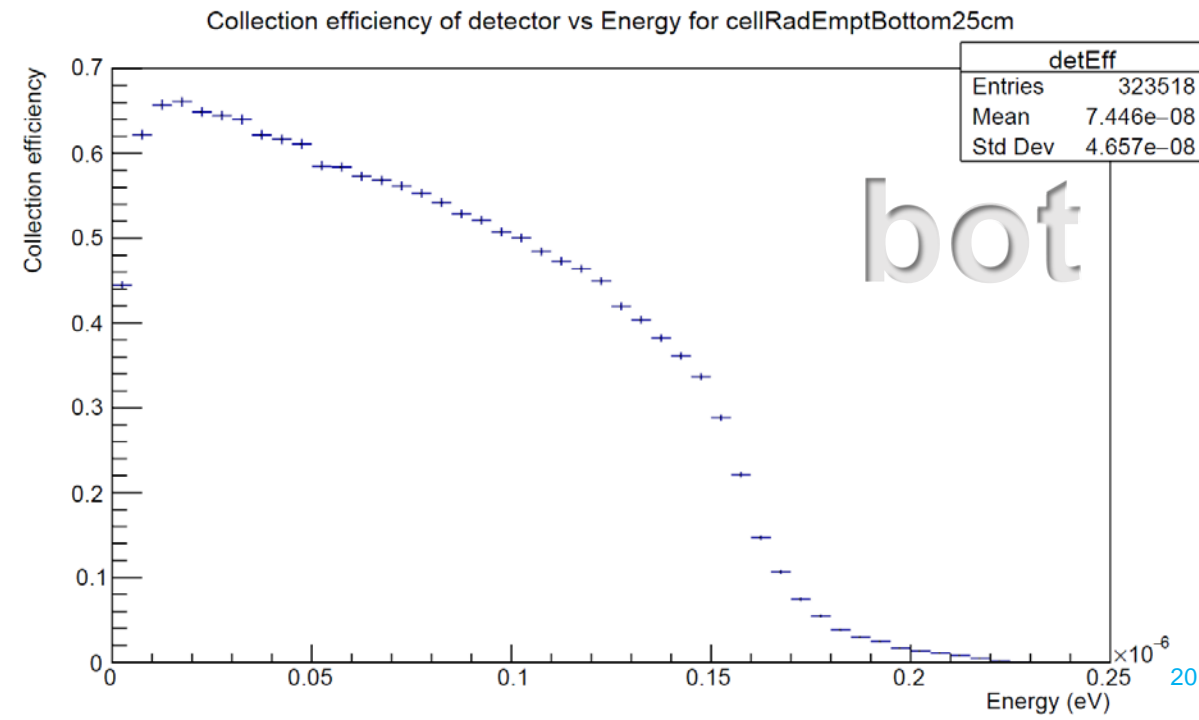
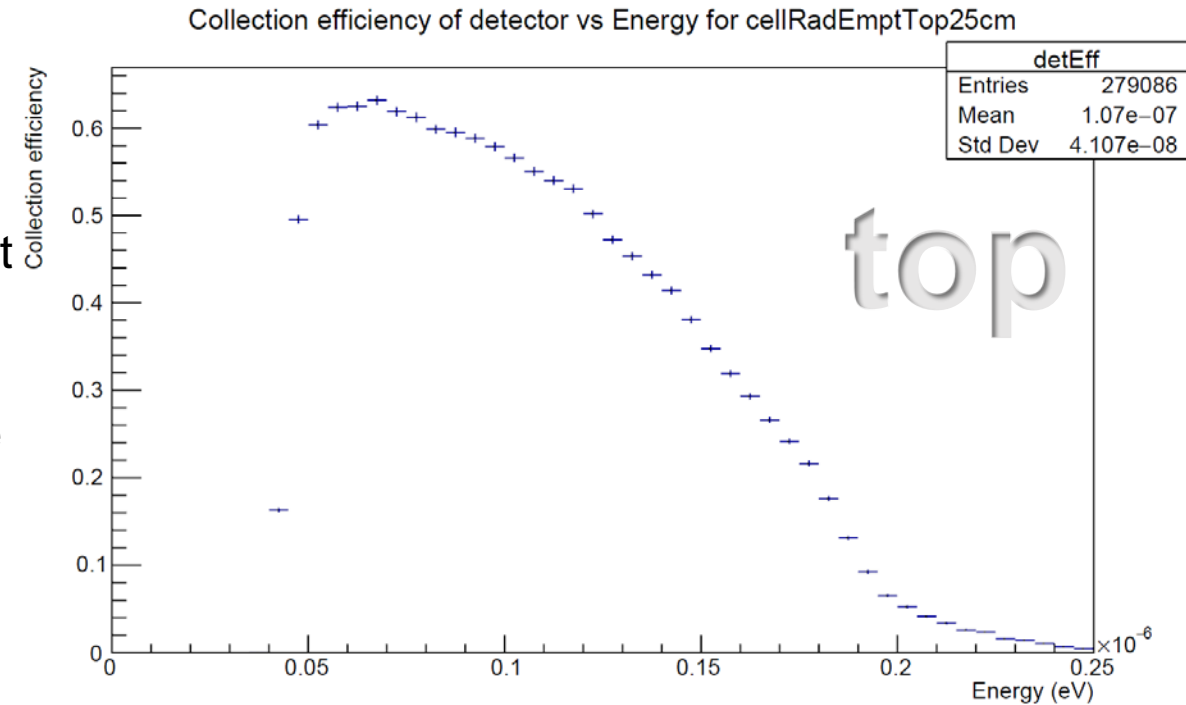
1. Spawn all UCN inside EDM cells at $T=0$ with a constant energy distribution
2. Store UCN with EDM cell valve closed for 300 s
 T_{Ramsey}
3. Record energy distribution every second



1. Spawn neutrons inside EDM cells at $T=0$ with constant energy distribution, EDM cell valve open and EDM switch connecting to detectors
2. Record energy distribution of neutrons collected in the detectors every second T_{count}



1. Spawn neutrons inside EDM cells at $T=0$ with constant energy distribution, EDM cell valve open and EDM switch connecting to detectors
2. Record energy distribution of neutrons collected in the detectors every second T_{count}



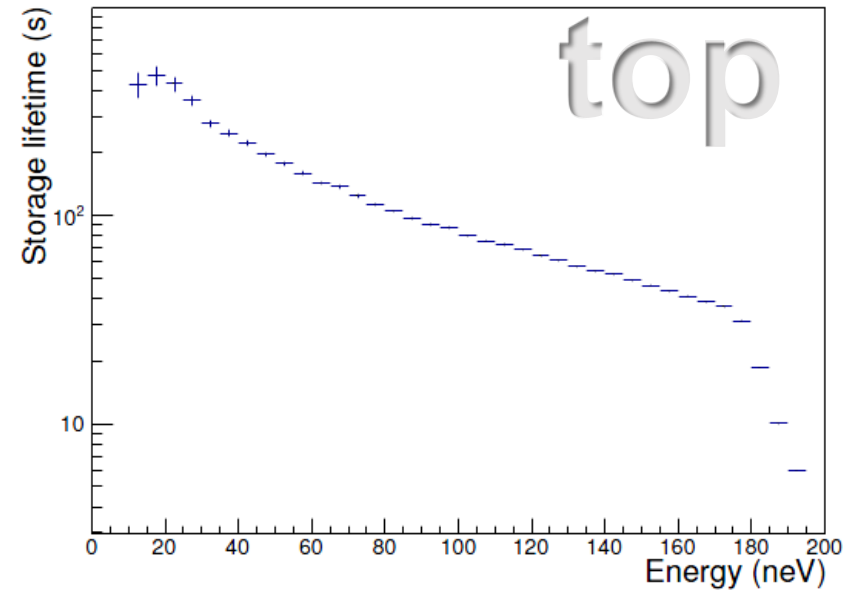
Optimal timings

- Accumulation time $T_{accumulate} = 26$ s
- Fill time $T_{fill} = 96$ s
- Storage time $T_{Ramsey} = 129$ s
- Counting time was $T_{count} = 88$ s

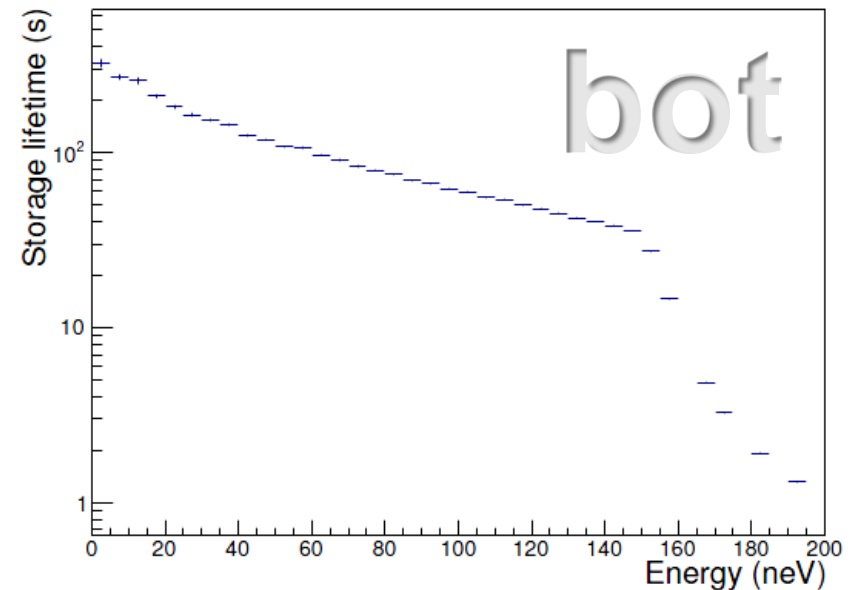
Conclusions

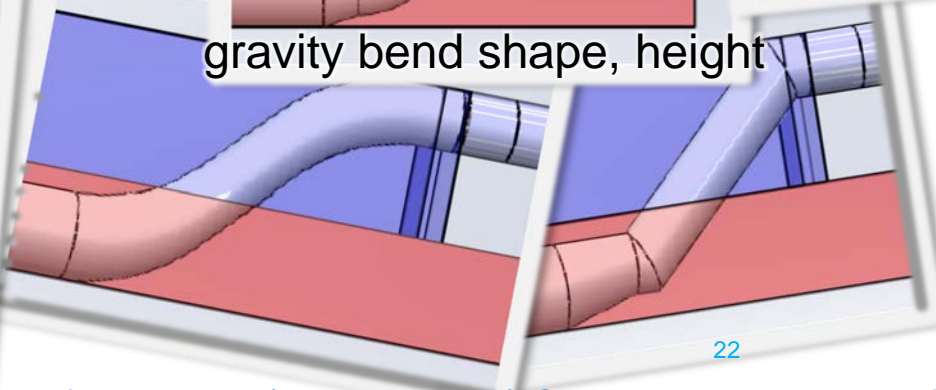
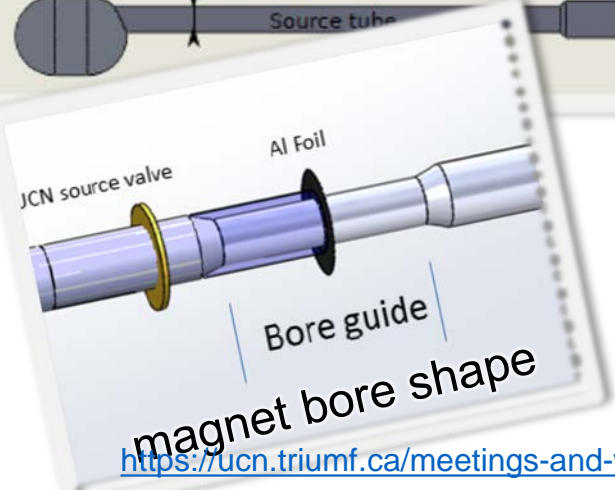
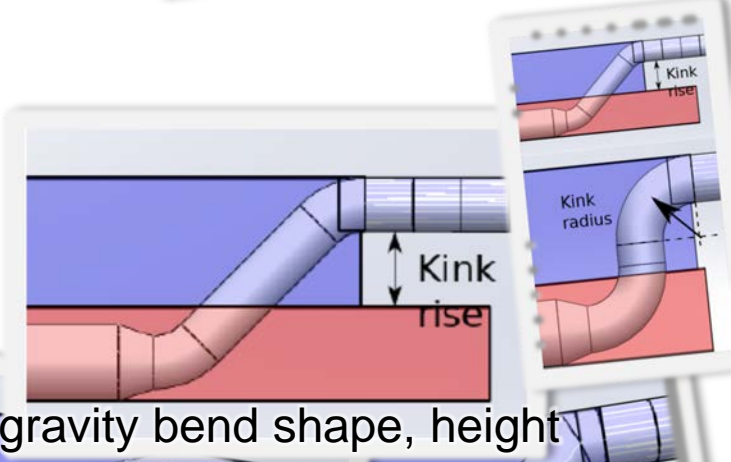
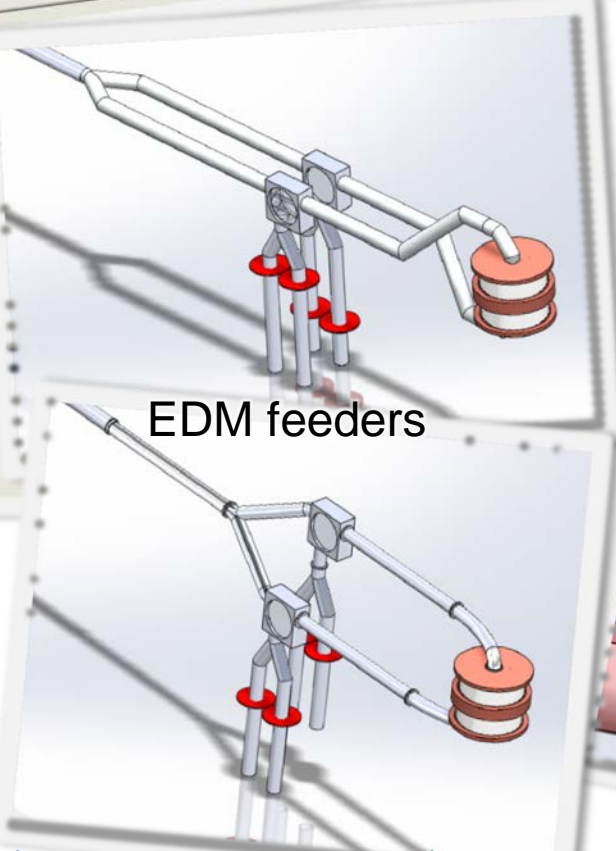
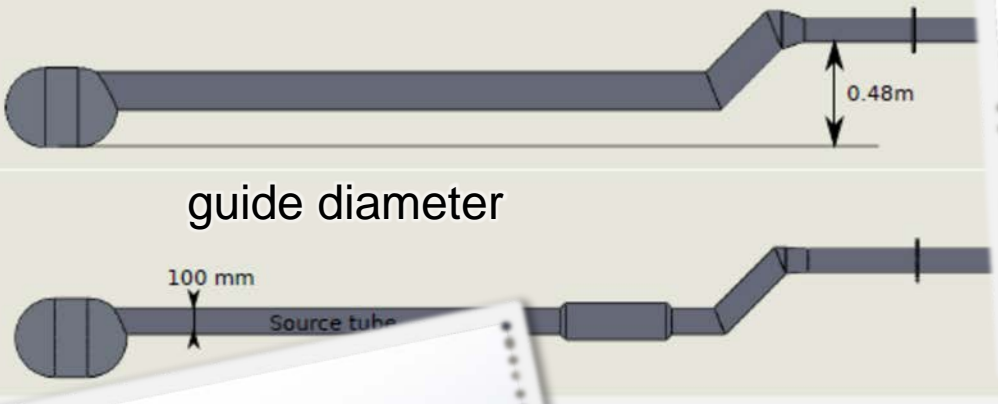
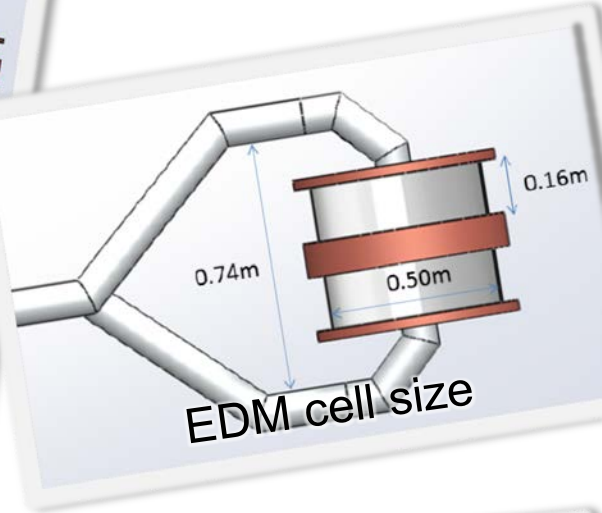
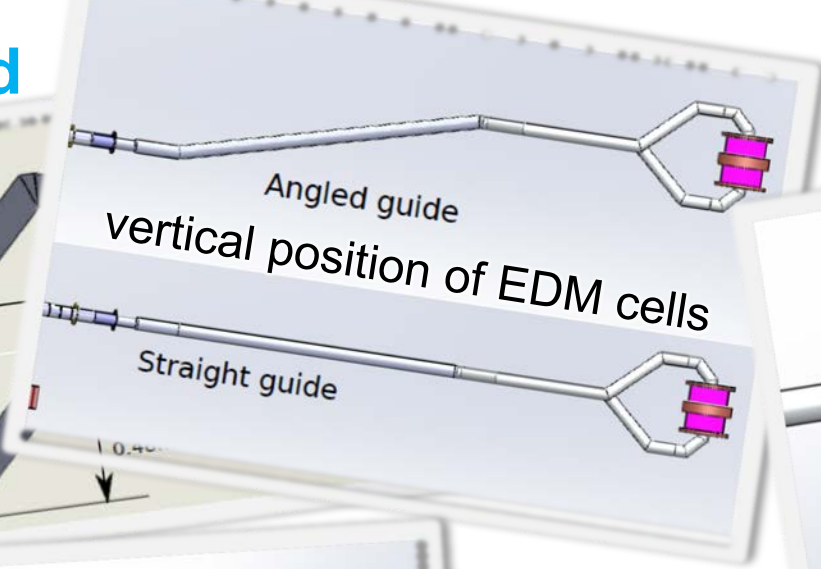
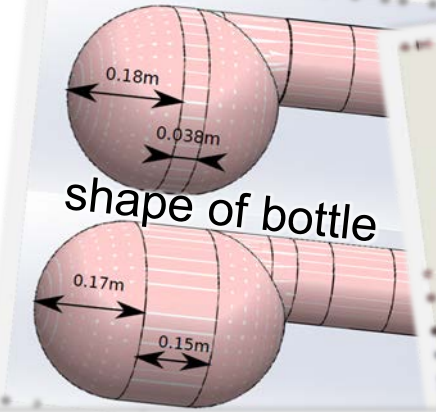
- These times are quite a bit longer than originally anticipated.
- Transport timings are longer for lower energy neutrons. These have
 - longer storage lifetime in EDM cells and
 - a better collection efficiency.
- This increases T_{Ramsey} and N_{det}

Top cell



Bottom cell

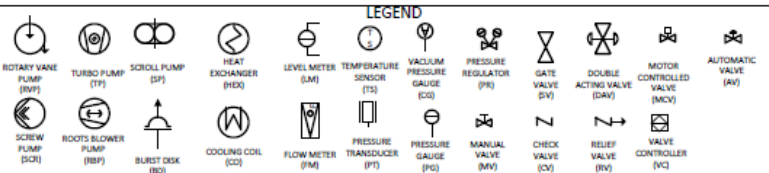
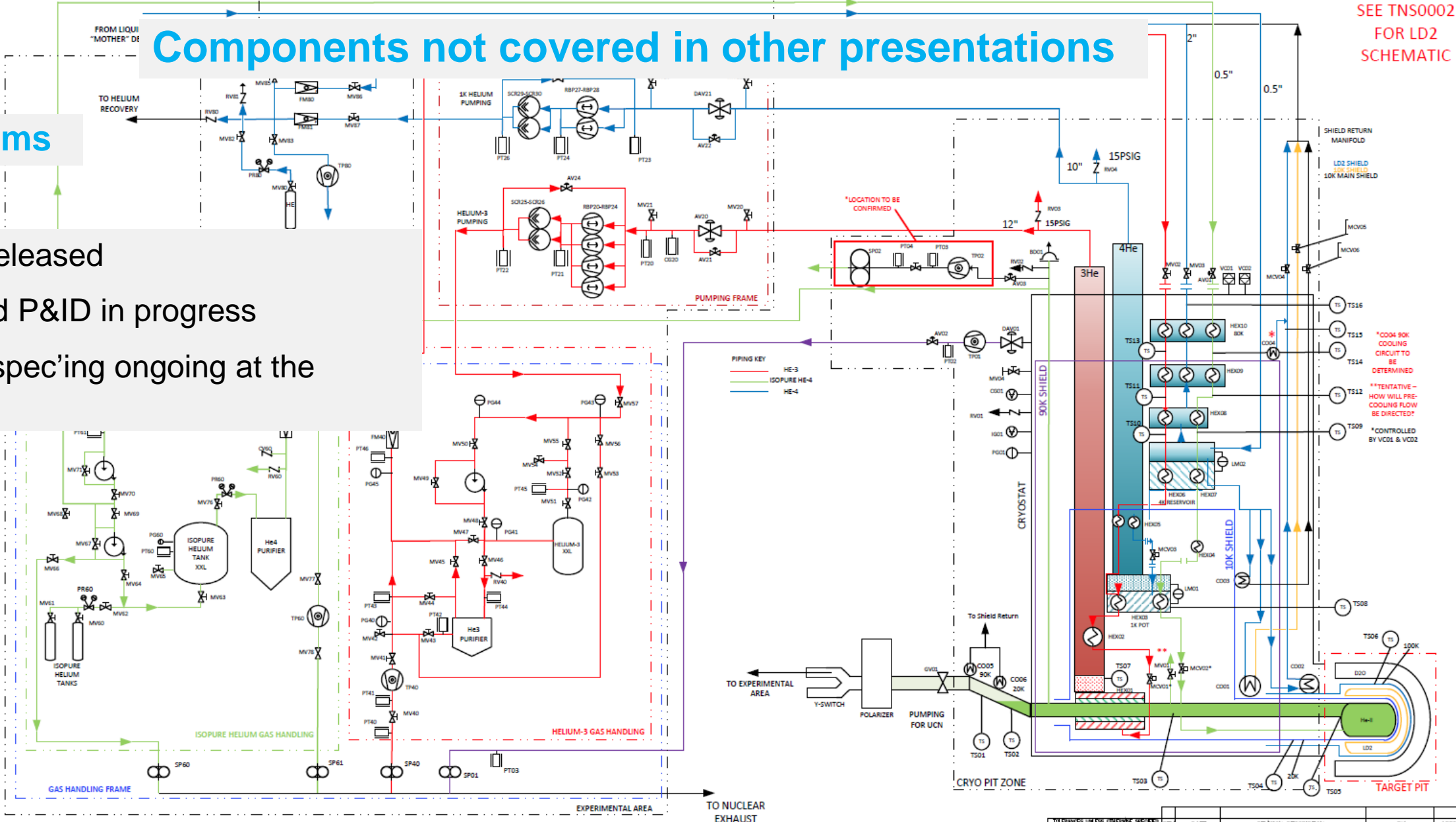




Components not covered in other presentations

He gas systems

- Initial P&ID released
- More detailed P&ID in progress
- Component spec'ing ongoing at the moment



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REV	DATE	REVISION DESCRIPTION	BY	APPD

TRIUMF Canada's particle accelerator centre
Centre canadien d'accélération des particules
4004 Héroux Rd., Vancouver, BC V6T 2A2, Canada

DRAFT
UCN HORIZONTAL SOURCE P&ID
UCN 2018

SCALE: 1:1
TNS0354
SIZE: D
SHEET: 1

He gas systems

- Initial P&ID released
- More detailed P&ID in progress
- Component spec'ing ongoing at the moment

Liquid helium transfer line

- 43 m total length, ~4 m elevation drop
- Capacity ~100 L/hr
- Heat load as low as possible: <3 W, 4.2 L/hr LHe loss
- LN₂ or return gas cooled shield
- Requesting support from TRIUMF's cryogenics group
- RFP planned by mid 2020

Helium pumping system

- Two systems required
 - **Natural helium (1K pot): 1.26 g/s at 5.4 Torr** (\$200k)
 - **Helium-3: 1.14 g/s at 2.38 Torr** (\$400k)
- Ideally both systems use the same pump models.
- Tender this spring
- Starting with subset of pumps

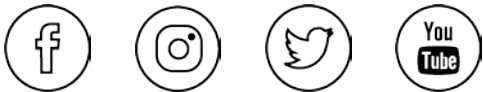
- We have solved nearly all major challenges posed by the TUCAN next generation source.
- We are making good progress and have achieved major milestones.
- We plan to install it in 2021 and perform first beam tests the same year.
- This is highest priority of the TUCAN collaboration!

We have very challenging and demanding 2 years ahead of us to have many different components come together on time!

Thank you
Merci

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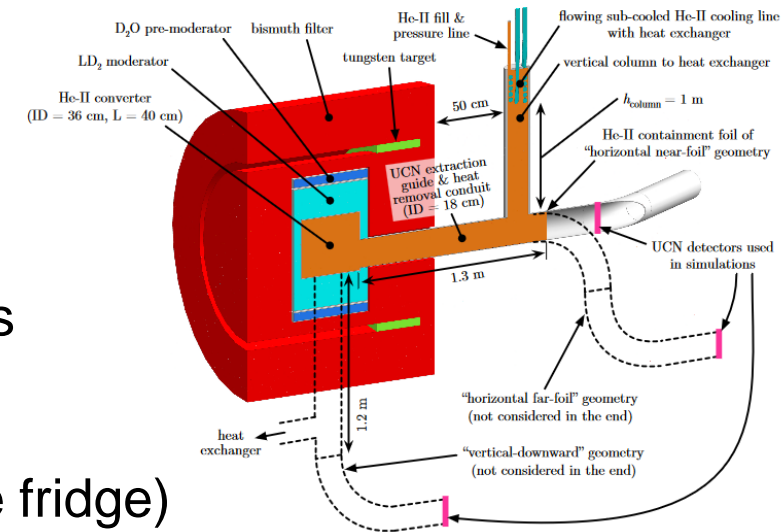
Some relevant numbers (compared to inverse geometry source)

TUCAN source (engineering stage)

- Production $1.4\text{-}1.6 \times 10^7$ UCN/s
- Source helium temp 1.03 K to 1.13 K
- Cooling power 10 W (3He fridge)
- Source storage lifetime 28 s
- Figure of merit $P\tau = 4.5 \times 10^8$
- Density in the source 3×10^3 UCN/cc
- Total number in the source 3×10^8 UCN
- Initial density in 70 l EDM expt 200 UCN/cc
- Counted at the end of cycle 2×10^6

Inverse geometry source (conceptual stage)

- Production 1.8×10^9 UCN/s
- Source helium temp 1.6 K
- Cooling power 100 W (4He fridge)
- Source storage lifetime 2 s
- Figure of merit $P\tau = 3.6 \times 10^9$
- Density in the source 5×10^4 UCN/cc
- Total number in the source 6.5×10^9 UCN
- Initial density in 100 l perfectly matched expt 10000 UCN/cc



<https://arxiv.org/abs/1905.09459>

Built 2012

liquefaction rate	50 l/h
UCN needs 2017	ca. 25 l/h
CMMS needs	Ca 15 l/h

1000l dewar

Linde
1610

recovery compressors

RSX compressor

He bag



1. Spawn neutrons inside EDM cells at $T=0$ with constant energy distribution, EDM cell valve open and EDM switch connecting to detectors
2. Record energy distribution of neutrons collected in the detectors every second T_{count}

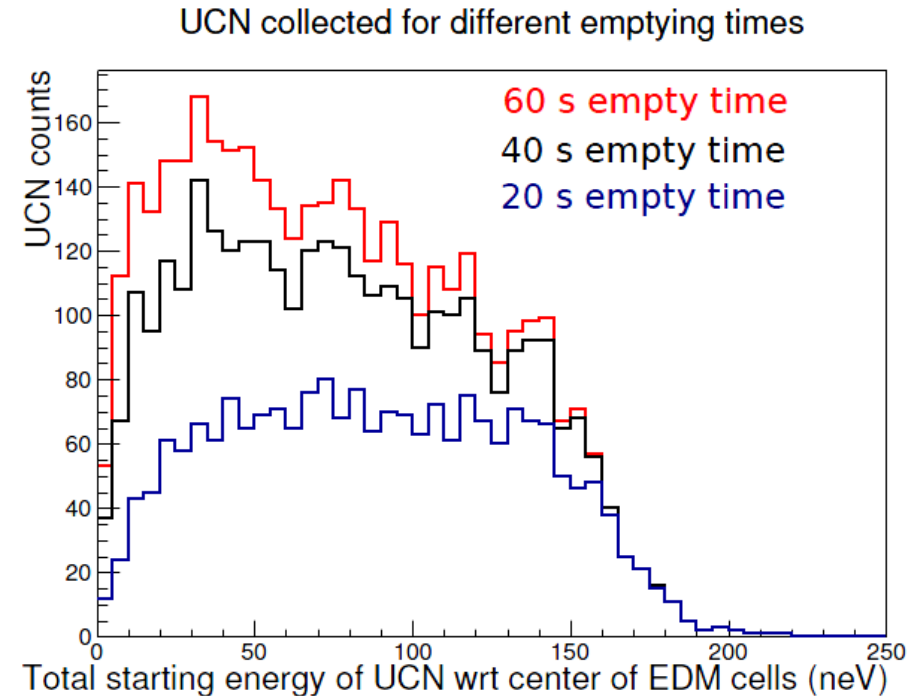


Figure 11: UCN collected by the detectors vs Total starting energy in the EDM cells in the cell emptying simulations. As emptying time increases the total number of UCN collected by the detectors increases and the average UCN energy decreases.

Parameter Studied	Values	Optimum	Spread from optimum (%)	Remarks	Concept Design
He bottle shape	Cyl (r=170 + 150), sph (r=180 + 38)	Spherical	~5%	~3% better	Cylinder
He bottle material	Al6061, Al2219, AlBeMet	AlBeMet	~25%	~17-20% better	Al6061
Bottle extraction	Low, mid, high	high	~13%	dbl kink ~ 5% better than high	High extraction
Source tube diameter (mm)	100, 125, 150, 180	150	~7%	150 ~ 4% better than 125	150
21.7KG HEX diameter (mm)	125, 150, 180, 200	180	~60%	(KG = 21.7) 180 ~ 50% better than 150, 200	148
35KG HEX Diameter (mm)	125, 148, 180, 200	148	~6%	148 and 125 are roughly the same	148
Funnel shape	Symmetric, asymmetric, eccentric	eccentric	~7%	eccentric ~ 4% better than Asymmetric	eccentric
Kink rise (cm)	18, 23, 28, 33, 38, 43	18	~ 8%	18 ~ 2% better than next best	18
Kink radius (cm)	15, 22, 29, 36, 43, 50, 57	no clear optimum	~ 0	no significant difference	20
Kink angle (deg)	45, 50, 55, 60, 65, 70, 75, 80, 85, 90	no clear optimum	~ 0	no significant difference	90
UCN guide diameter (mm)	86, 95, 100, 125	125	~10 %	95 ~ 7% better than 86, ~ 2% worse than 125	100
Bore guide diameter (mm)	40, 45, 50, 55, 60, 67	67	~15 %	200 mm fixed length	70
Spider location	On 45 deg kink, on and out side 90 deg kink	no clear optimum	~1 %	no significant difference	out side of 90deg kink
Cell radius (cm)	18, 20, 22, 25, 28, 30, 40, 50	50	~100 %	30cm ~ 20% better than 25cm	25

$$\sigma(d) = \frac{\hbar}{2\alpha E T_{Ramsey} \sqrt{N_{det}}}, \quad (1)$$

where

$$\alpha = \alpha_0 * e^{-t_{EDM}/T_2 - (t_{wait} + 2*t_{\pi/2})/T_1} * \epsilon_{depol} * P_{analyzer}$$

with an initial visibility of $\alpha_0 = 0.95$, depolarization (5 %, $\epsilon_{depol} = 0.95$), efficiency of the spin analyzers ($P_{analyzer} = 0.90$). For the simulations:

$$N_{det} = N_{coll} * \epsilon_{det} * 0.5 * P_{real}/P_{sim} * e^{-t_{storage}/\tau_{Xe}},$$

where $\epsilon_{det} = 0.90$ detector efficiency, and N_{coll} includes

$$N_{surv} = \sum_E N_{det}(E) * e^{-t_{storage}/\tau(E)}$$

The cycles to reach a sensitivity of 1×10^{-27} e · cm is given by

$$CTR = \left(\frac{\sigma_d}{8 * 1 \times 10^{-27}} \right)^2 \quad (2)$$

The cycles per day are thus given by:

$$CPD = \frac{t_{stable}}{8 * (t_{irrad} + t_{fill} + t_{EDM} + t_{empty}) + 2 * t_{flipPol} + t_{degauss}/10} \quad (3)$$

$$days = \frac{CTR}{CPD}$$

TUCAN UCN source pumping systems

Natural helium (1K pot): 1.26 g/s at 5.4 Torr

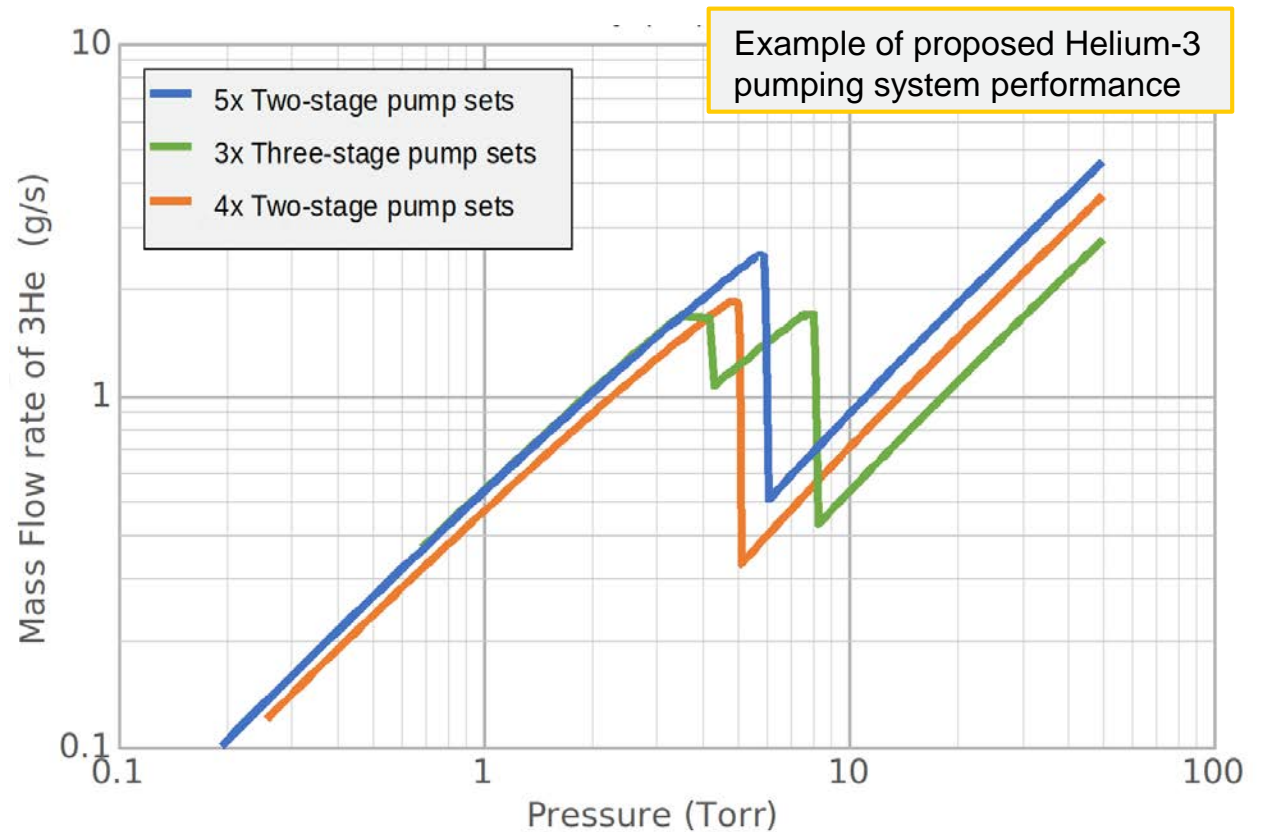
- well known pumping performance, low risk
- cost about 200 kCAD

Helium-3: 1.14 g/s at 2.38 Torr

- pumping performance only estimated
- minimize additional helium-3 for purges
- cost about 400 kCAD
- ideally both systems use the same pump models

Status

- discussion with three suppliers, 1-2 promising proposals
- TRIUMF conceptual design review in May 2019
- preparation of RFP ongoing
- approach to purchase minimal system first (possibly for Helium-3 only, use current pumps for Natural helium)



TUCAN UCN source liquid helium supply line

Natural helium supply

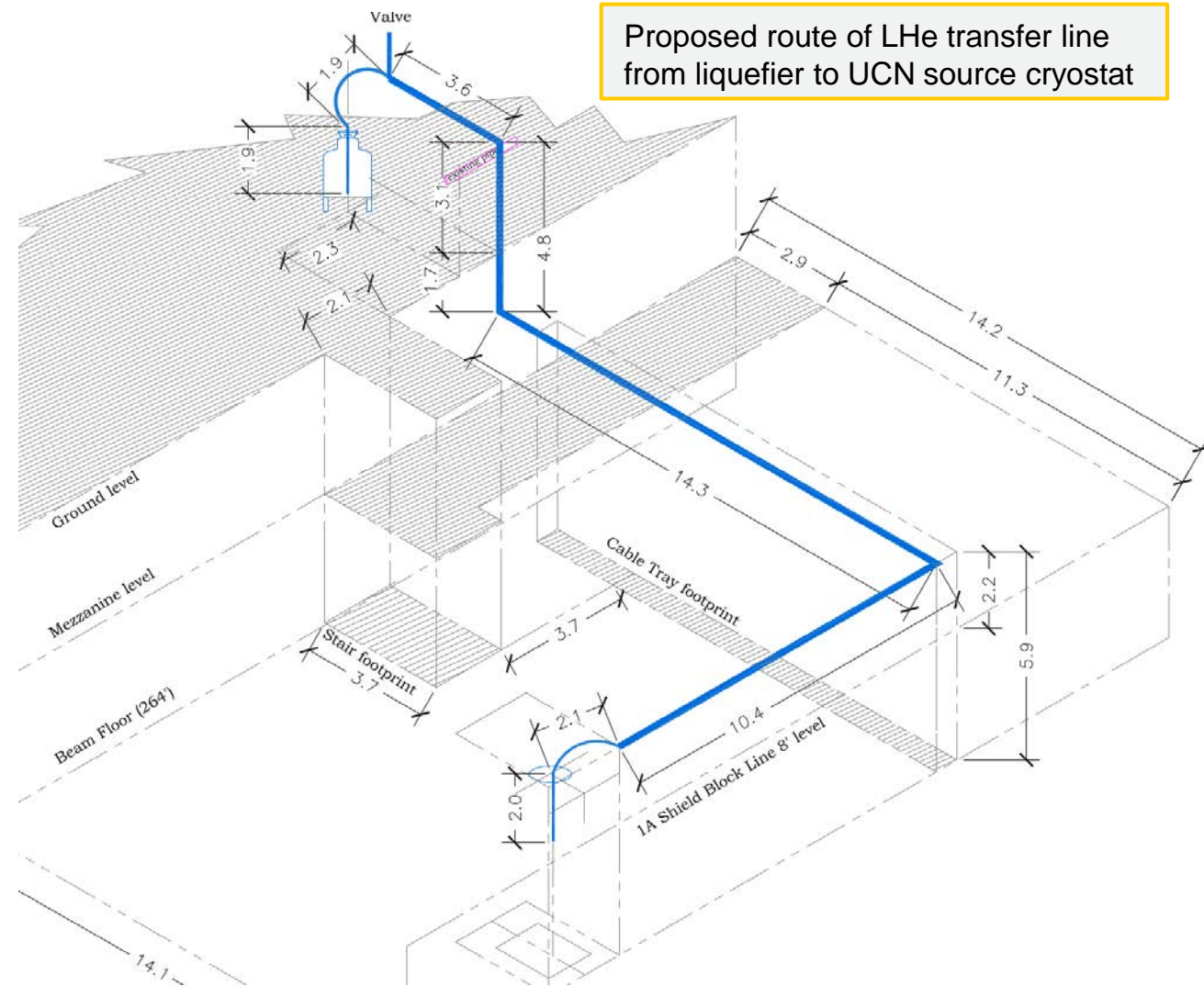
- liquefier production currently 50-55 L/hr
- Full, reliable operation requires upgrade of production rate and mother dewar capacity

Natural helium transfer line

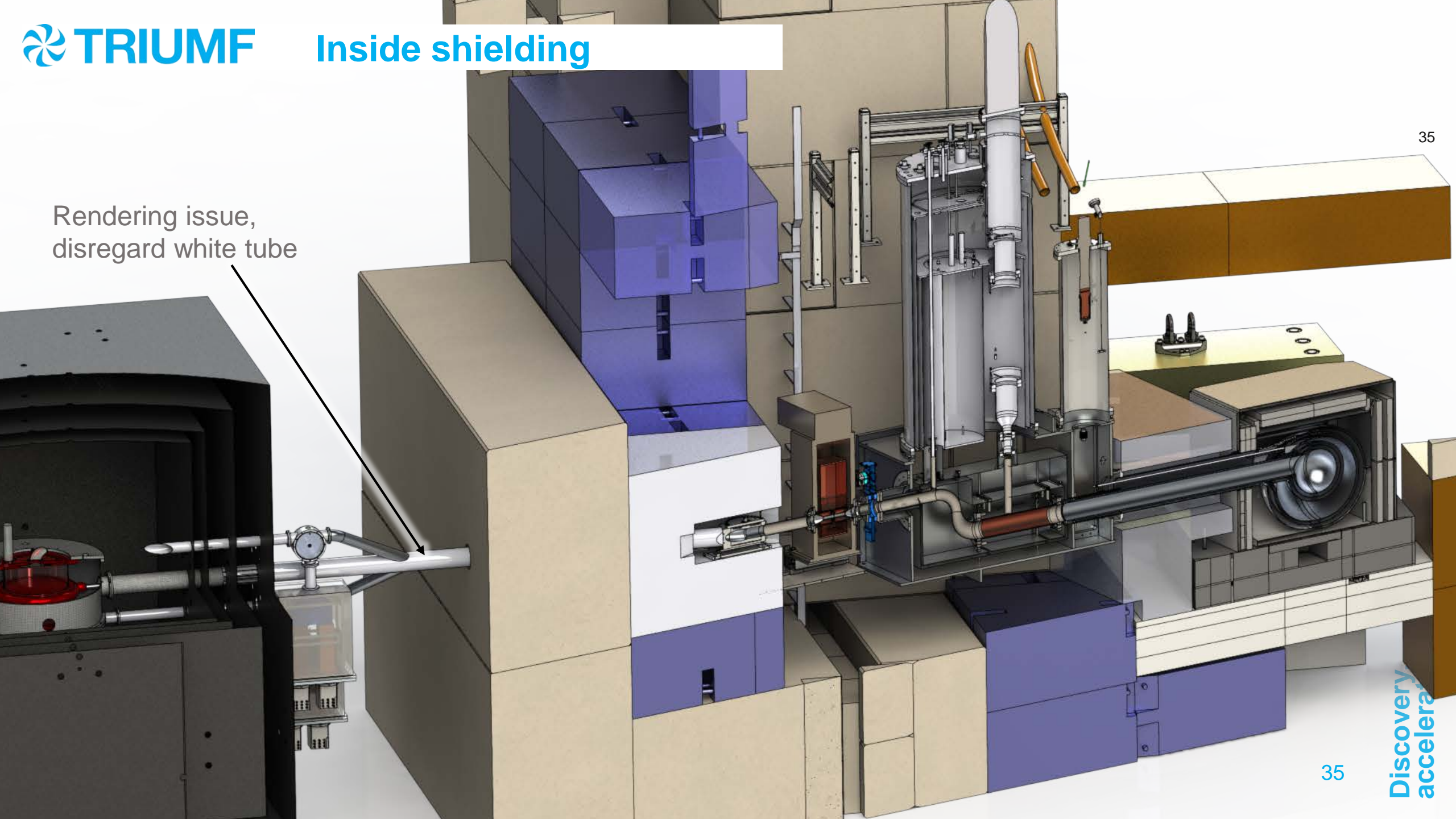
- 43 m total length, ~4 m elevation drop
- UCN source avg consumption
10W, 35% duty: 31 L/hr
- LHe supply line capacity ~100 L/hr
- Heat load <3 W, 4.2 L/hr loss (as low as possible)
- LN2 or return gas cooled

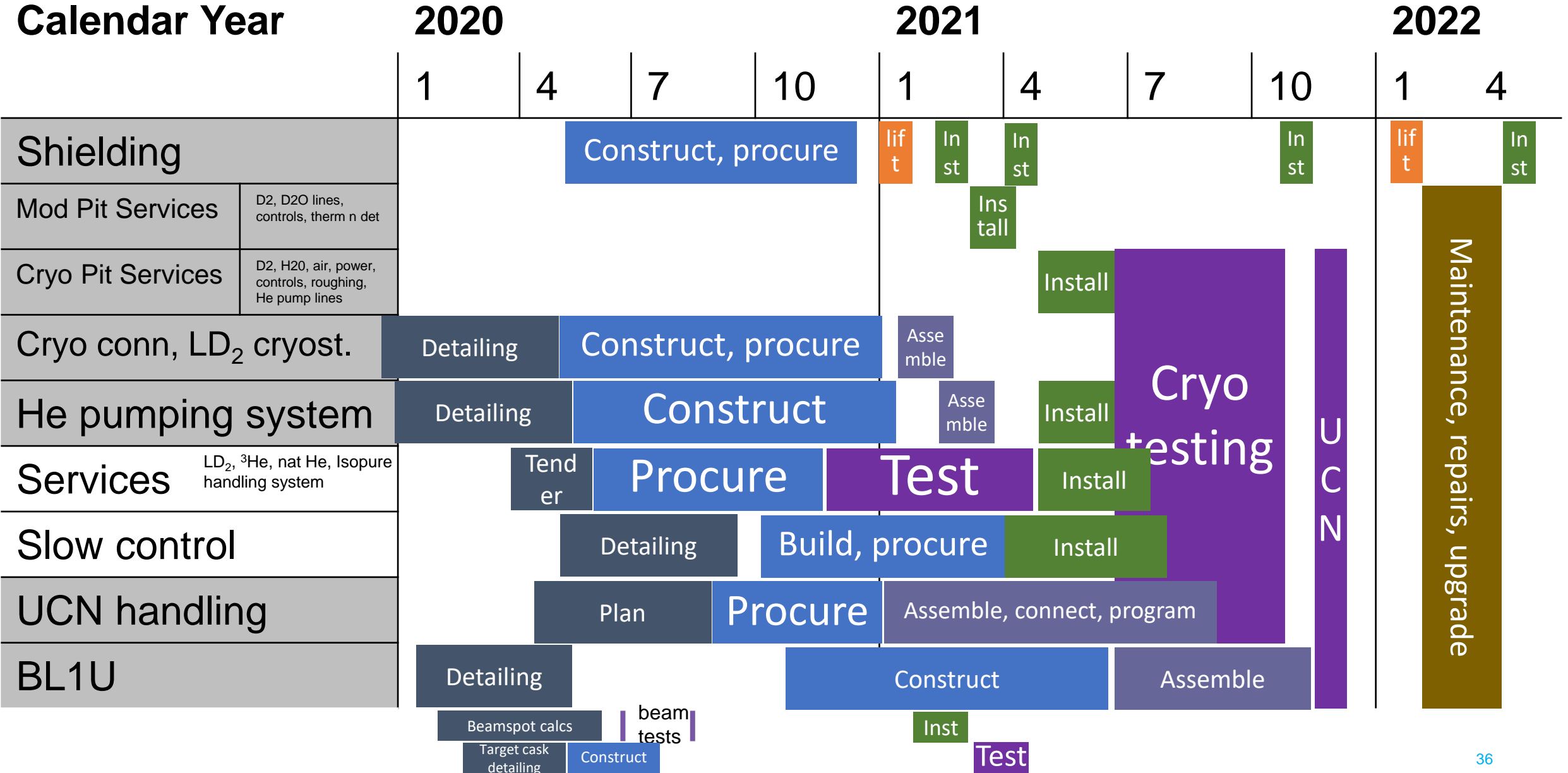
Status

- Request support from TRIUMF's cryogenics group
- RFP planned by mid 2020



Rendering issue,
disregard white tube



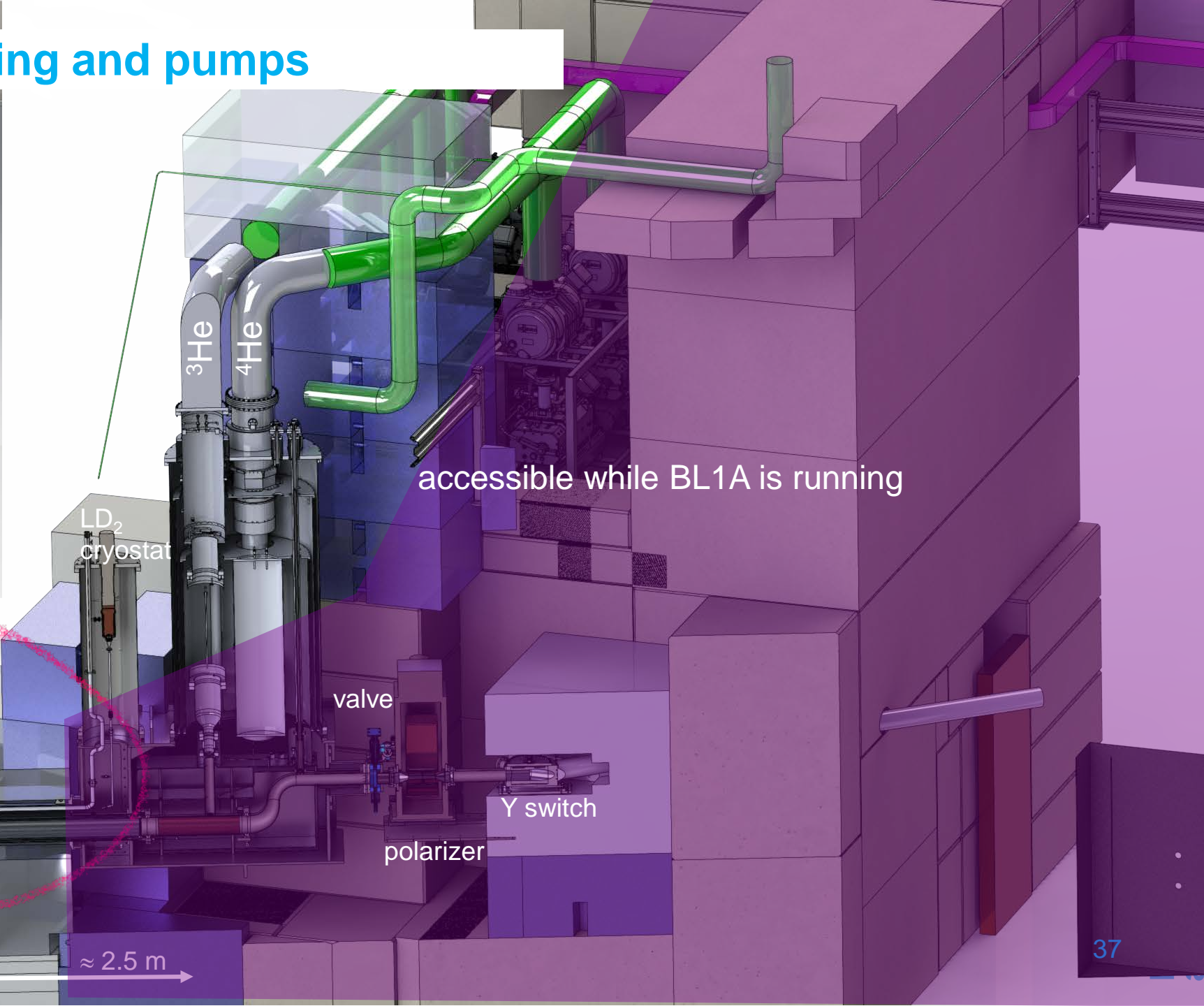


Gray shaded systems are inside the biological shielding.



BL1A shielding line

Has to be installed during shutdown



accessible while BL1A is running

≈ 2.5 m

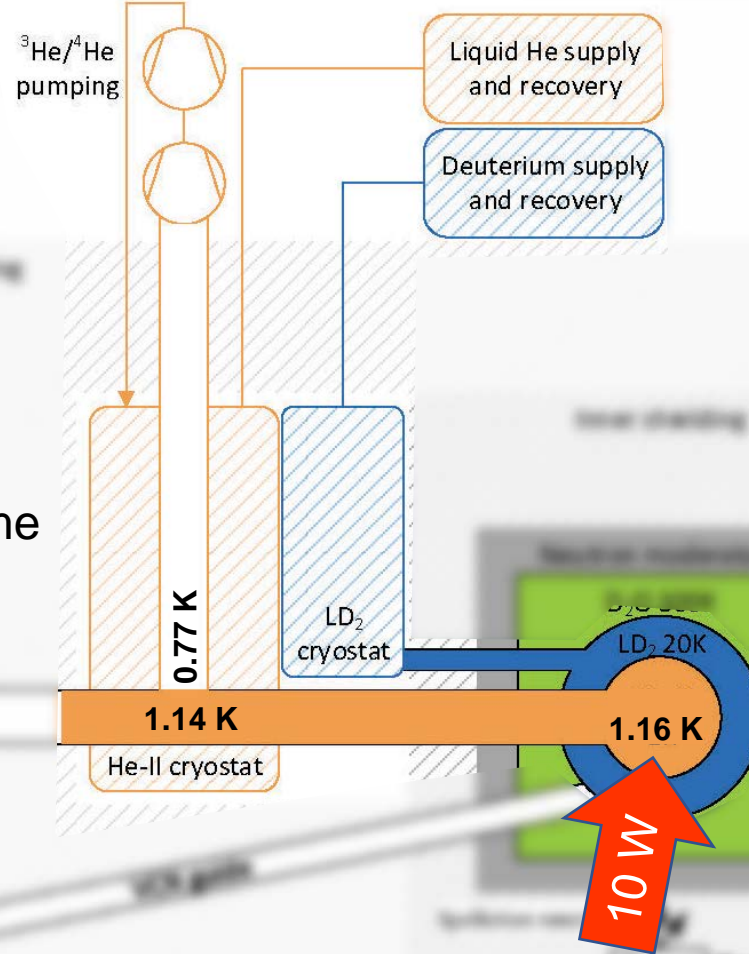
Cam Marshall

Shinsuke Kawasaki Ryohei Matsumiya Takahiro Okamura

Cold moderator: LD2

- Well known (scattering kernels)
- Among the best moderating performances
- Liquid (no burping)
- **Explosive**

Safety concept will be laid out. Volume < 150 liquid liters.



0.25 W static load, $K_0=22$, $a=2.6$, VanSciver

Converter cryostat: ^3He pumping

- Best cooling performance < 1 K
- Proven technology
- Own expertise
- Pressure drop in pumping duct manageable.
- Reasonable pumps required.
- **Uncertainty in surface and superfluid helium conductivity**

These uncertainties have been studied and are being experimentally tested.

Main disadvantages of ^4He direct pumping:

- **huge pumping power**
- **pressure drop very critical**

Analytical model useful to study many more parameter options than possible in simulation.

This is taken into account...

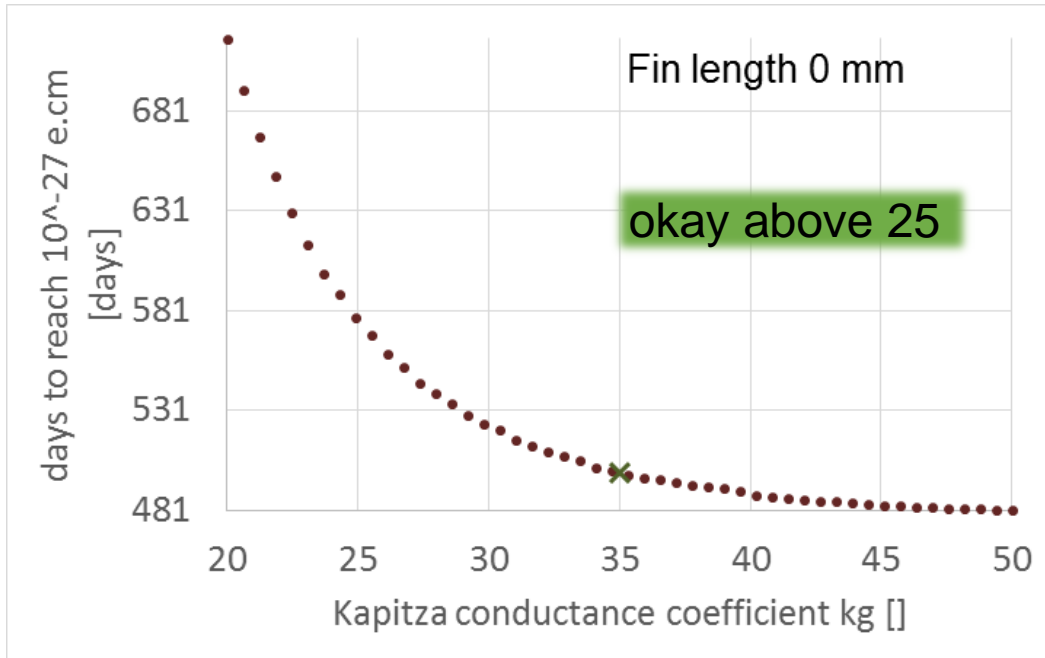
- UCN production/heat input from MCNP simulations
- Cryostat performance (pumps, pressure drop, HEX, heat conductivity)
- Neutron storage lifetime in source (He liquid + vapor)
- Phase space reduction due to wall Fermi potential and height differences
- Dilution of neutron "gas"
- Simple model of Ramsey cycle
- Probable stable daily measurement period
- Times for E field change, degaussing etc



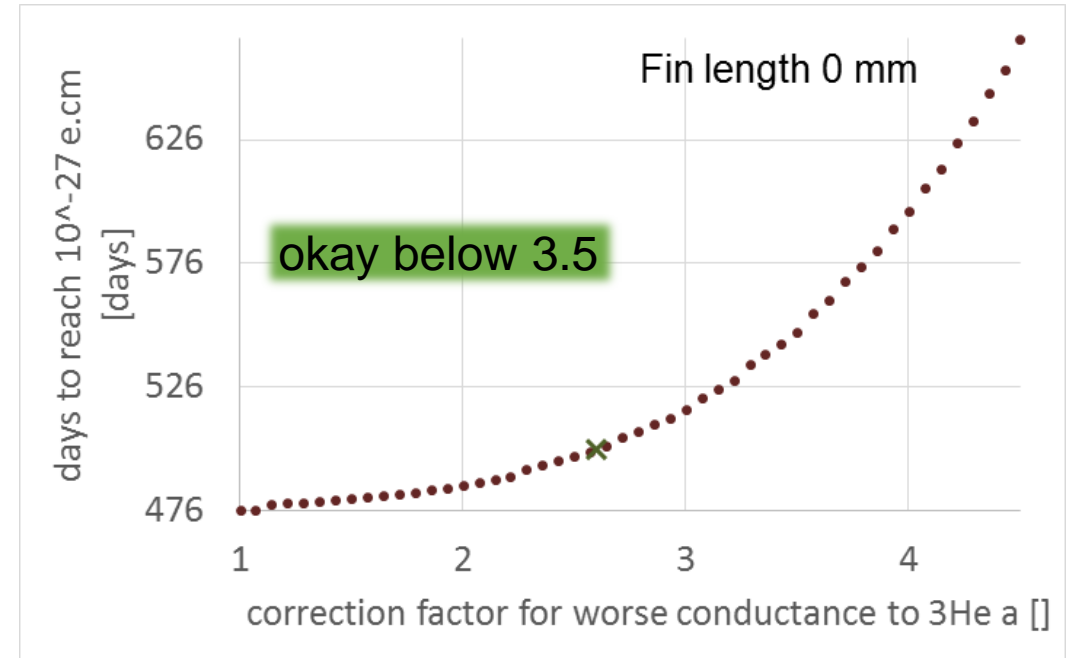
This is not... or not so well...

- Magnetic field of polarizer (it is in MC)
- Transport is only modelled via loss per meter, bend, foil etc
- Depolarization of UCN during transport (assuming 5% total)

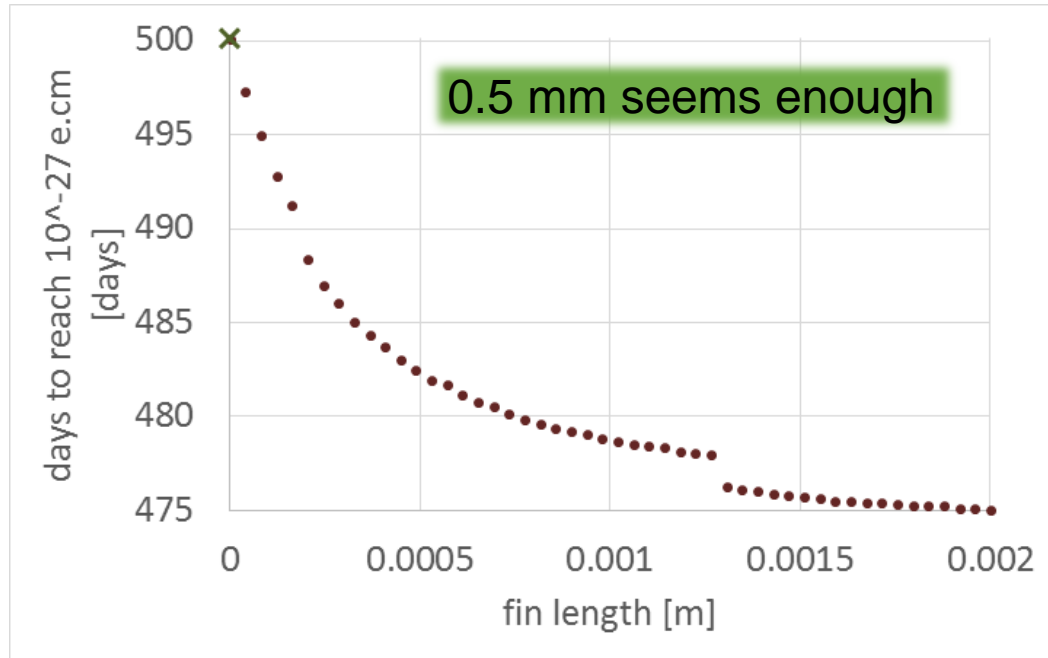
Kapitza resistance parameter K_G



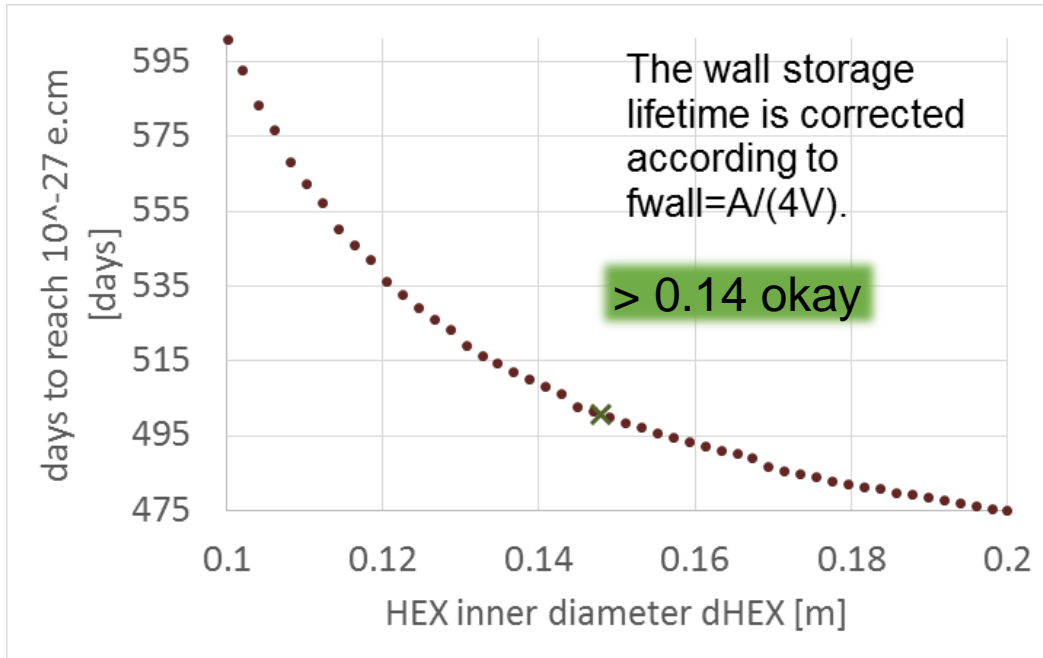
^3He Kapitza correction factor



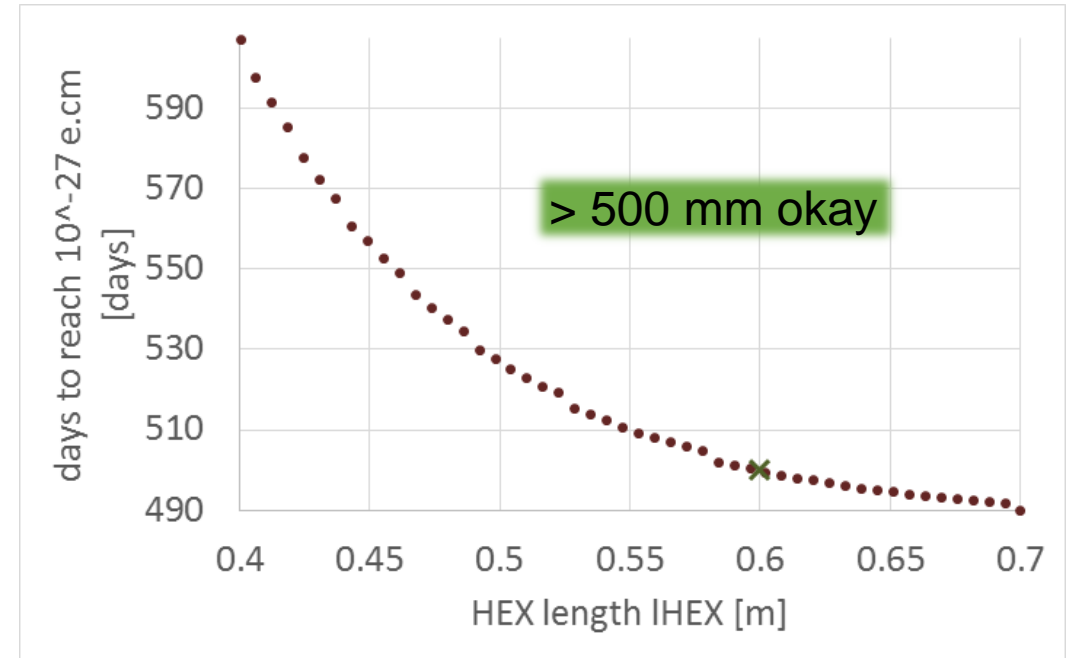
Fin length



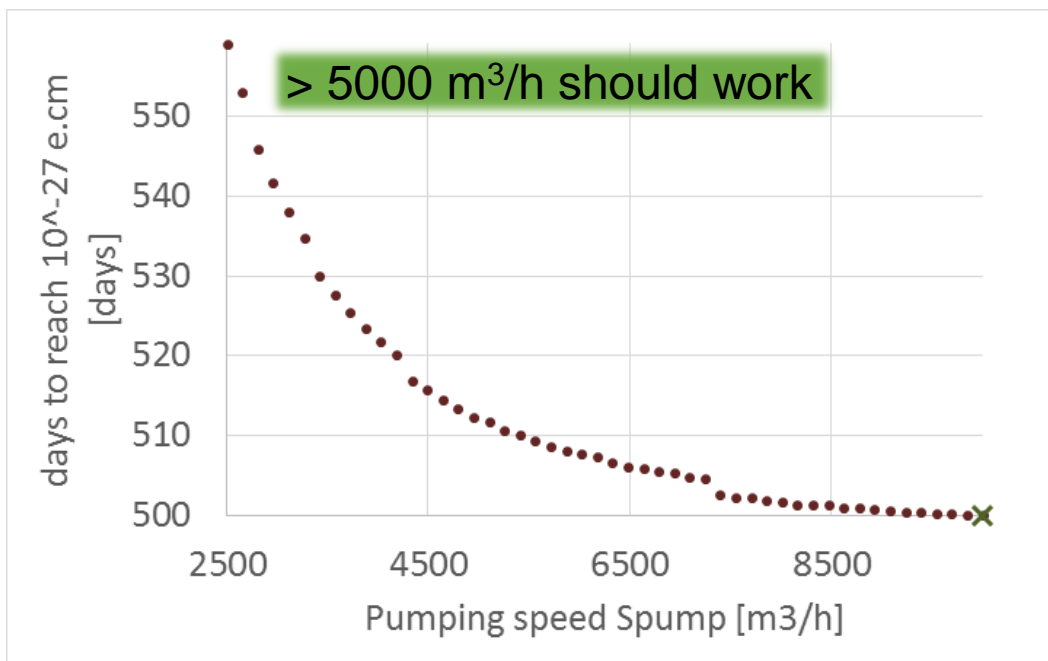
HEX1 inner diameter



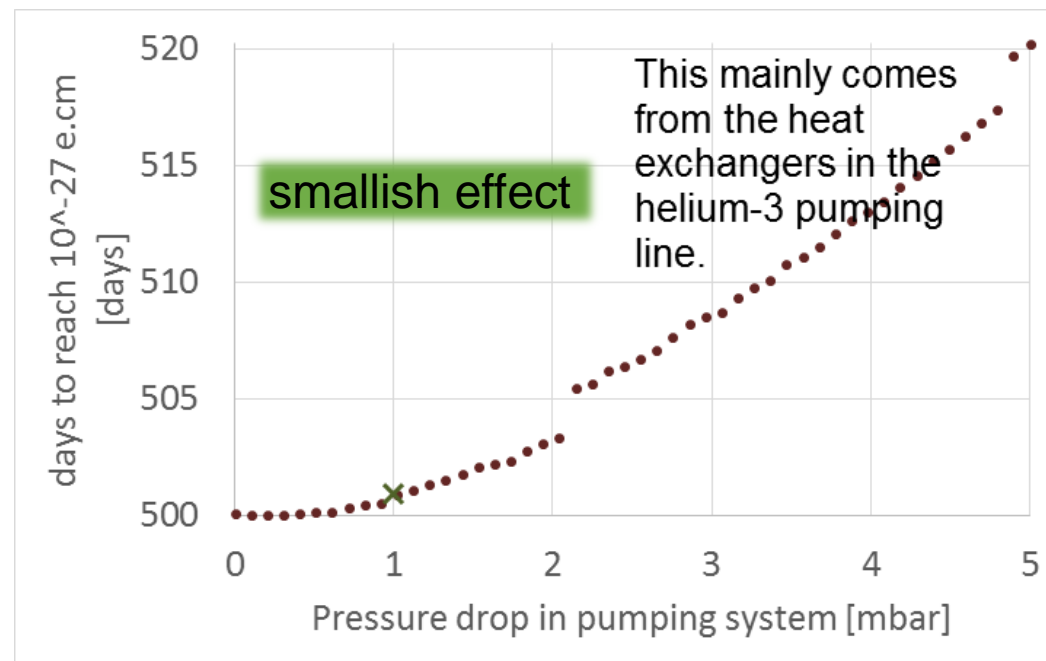
HEX 1 length



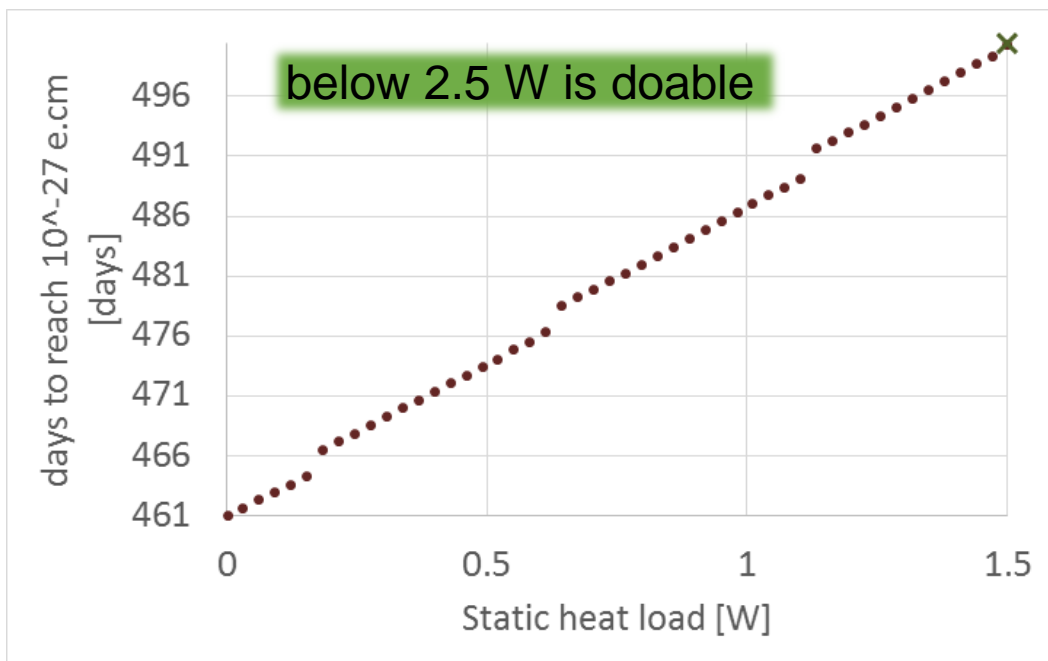
Pumping speed



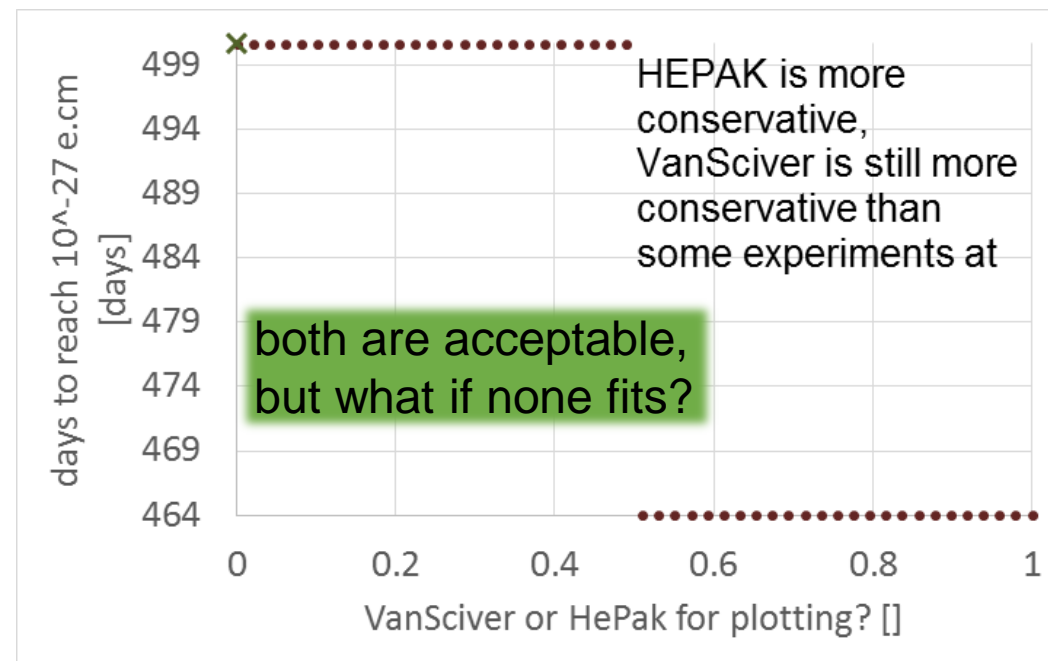
Pressure drop in helium-3 pumping line



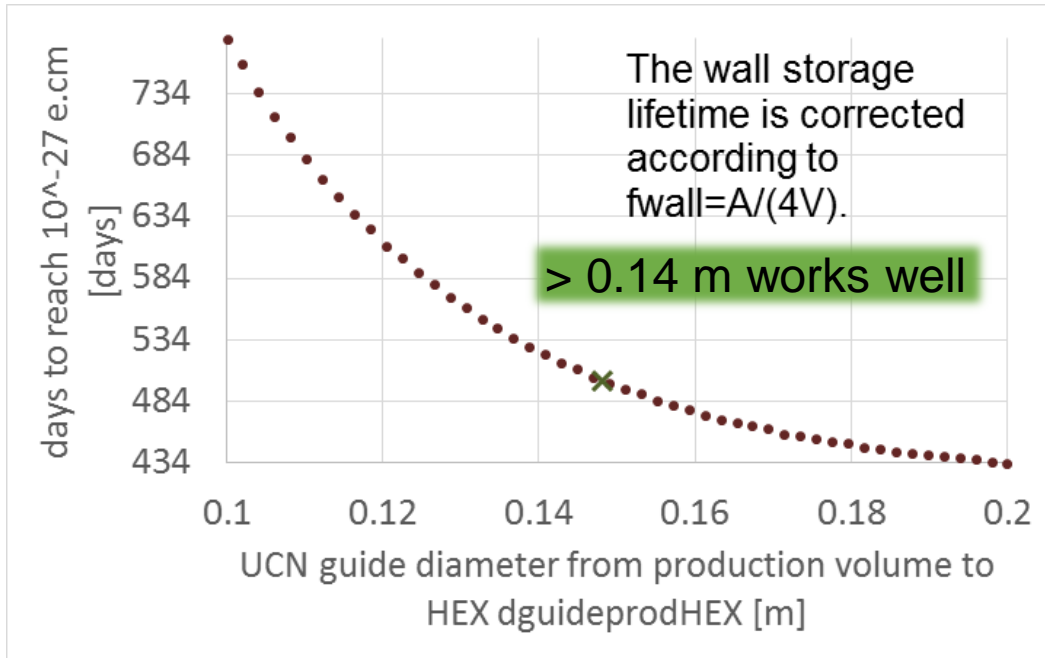
Static heat input



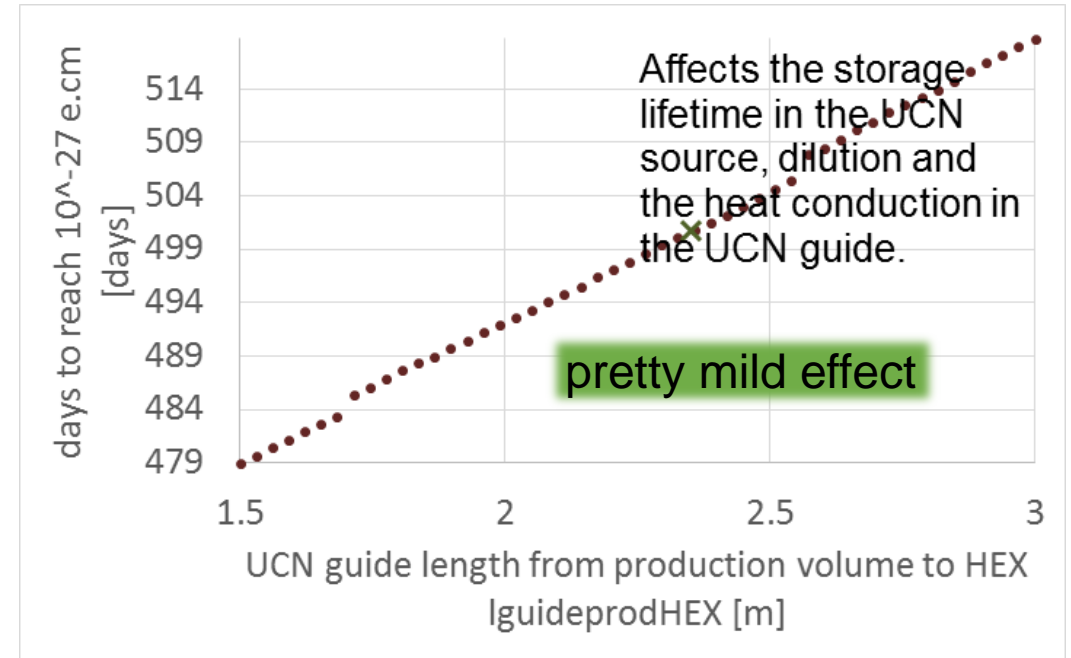
Model dependence



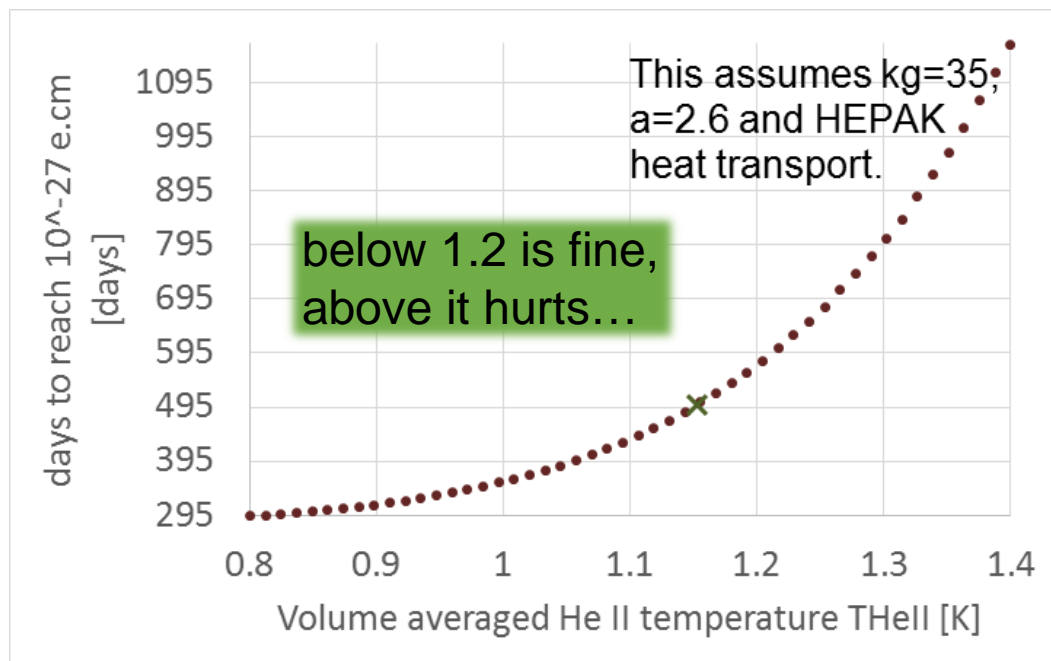
UCN guide and heat conduction channel diameter



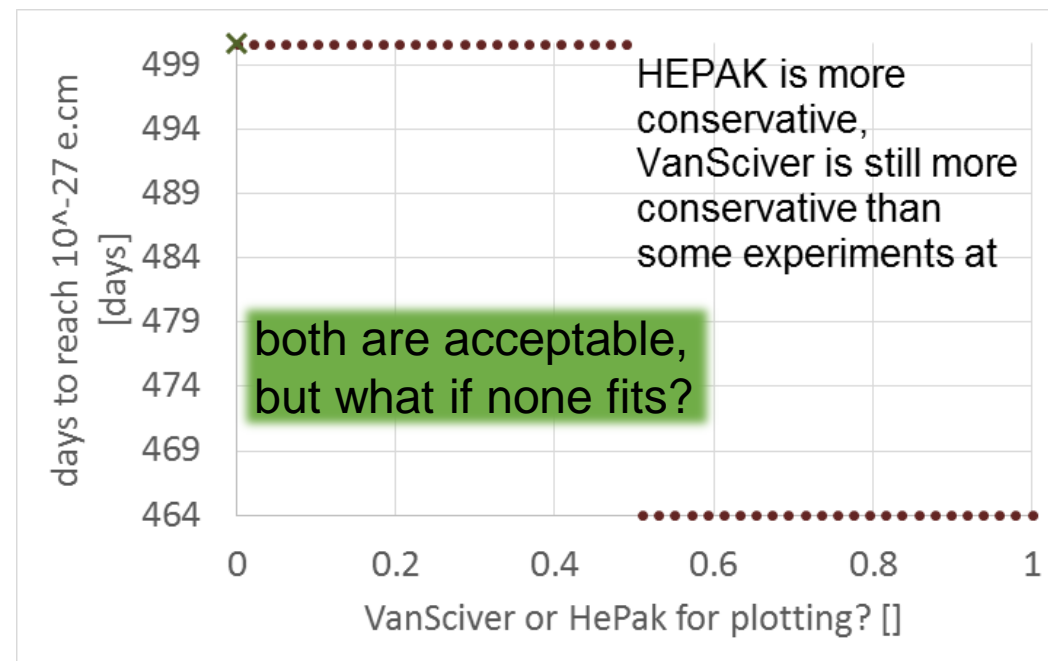
Length of the same



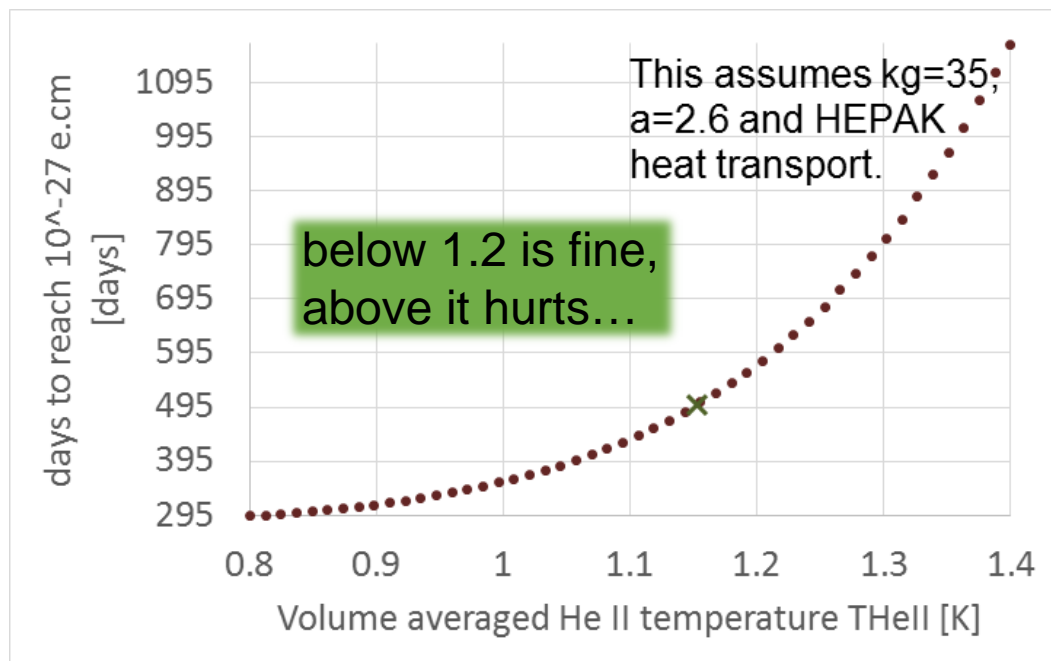
Volume averaged isopure helium temperature



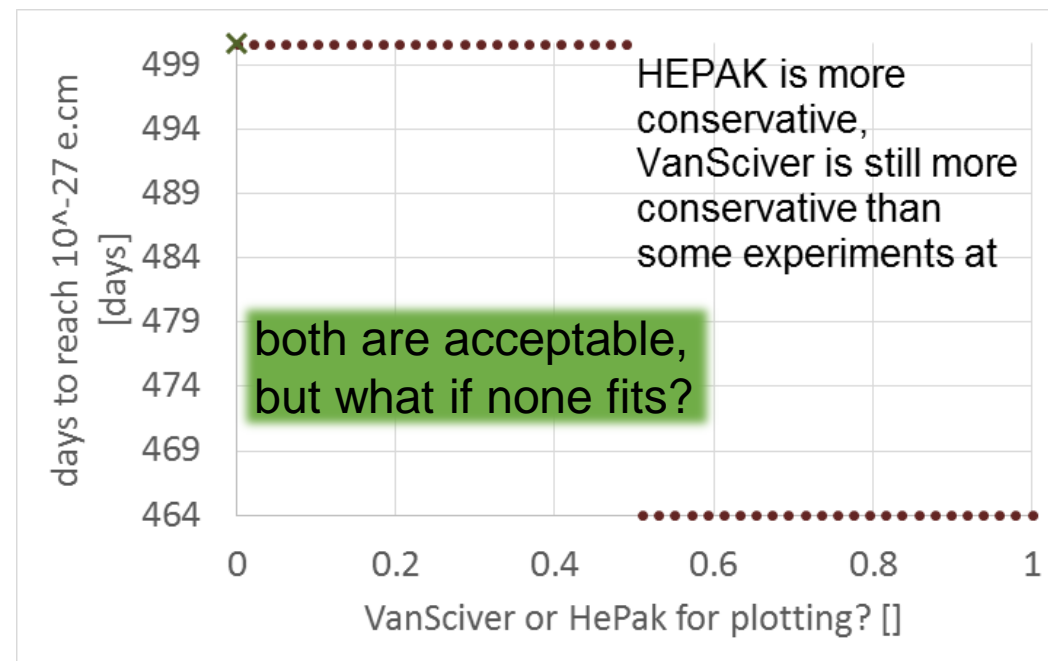
Model dependence



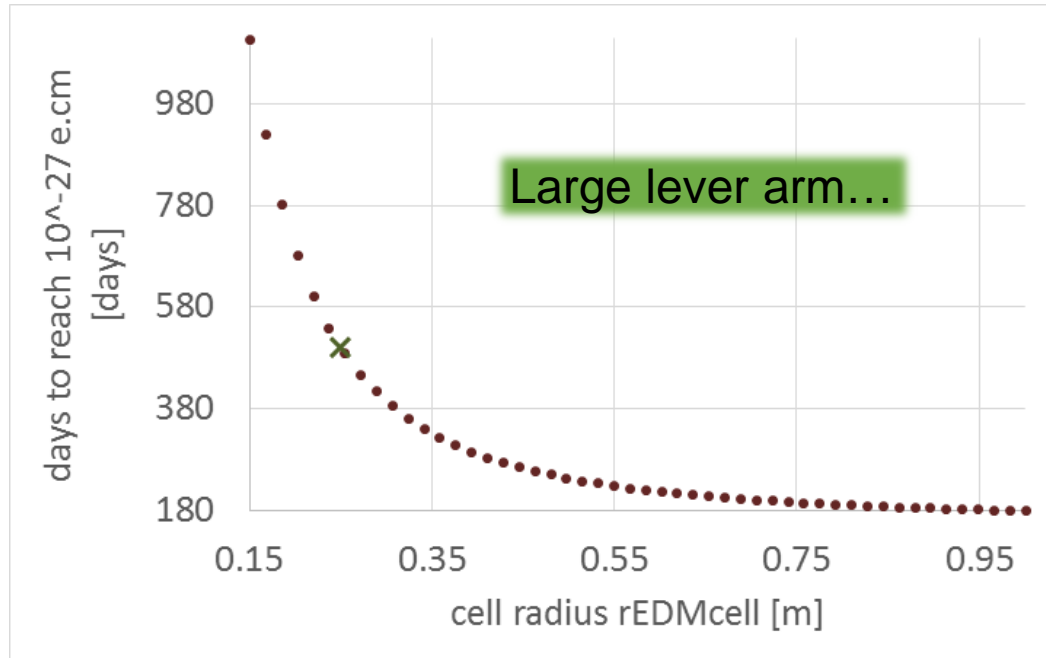
Volume averaged isopure helium temperature



Model dependence



EDM cell radius



EDM cell height (E field kept at 13 kV/cm)

