

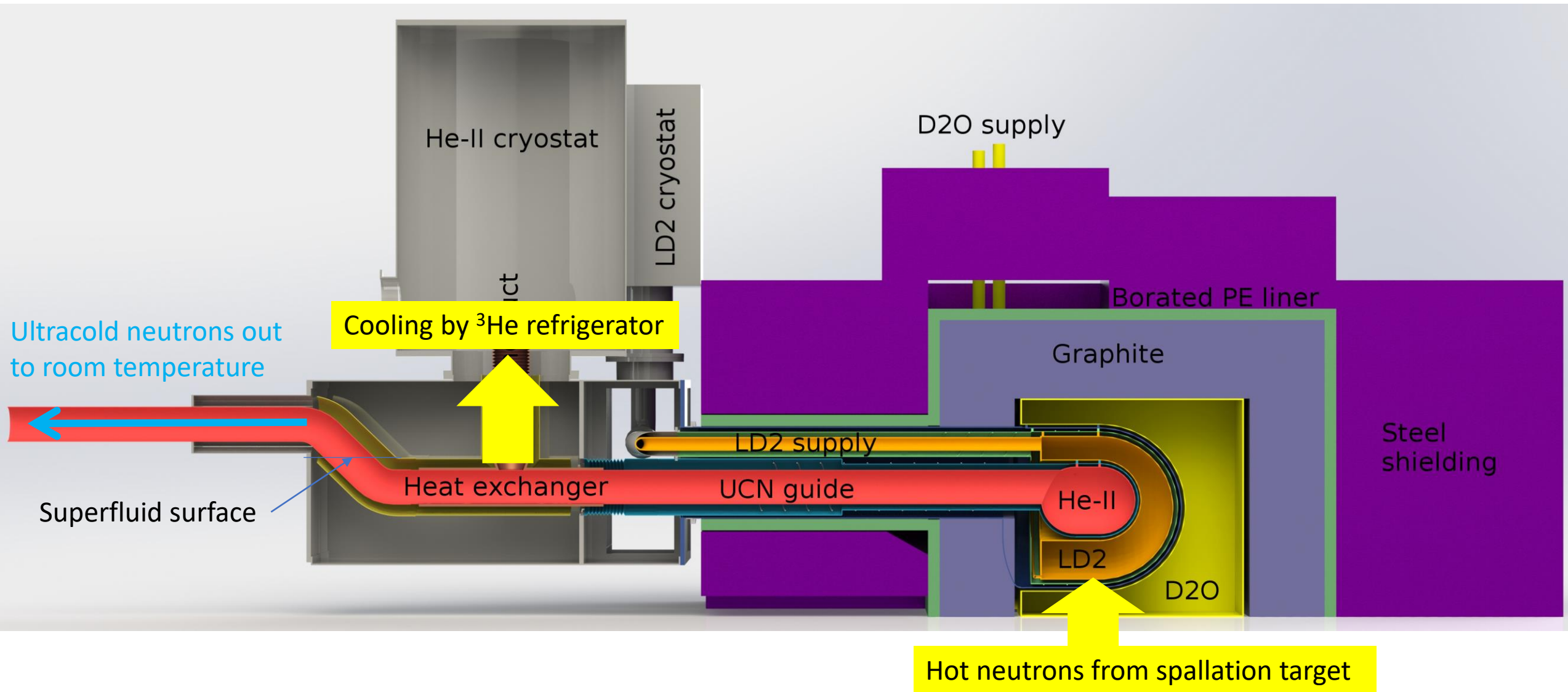
Time-dependent Cryogenic Models of the TUCAN Source

S. Stargardter

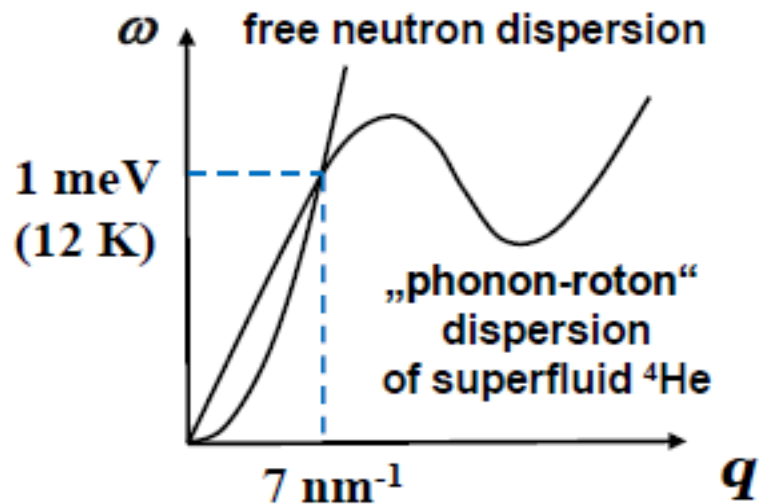
For the TUCAN collaboration

February 5, 2021

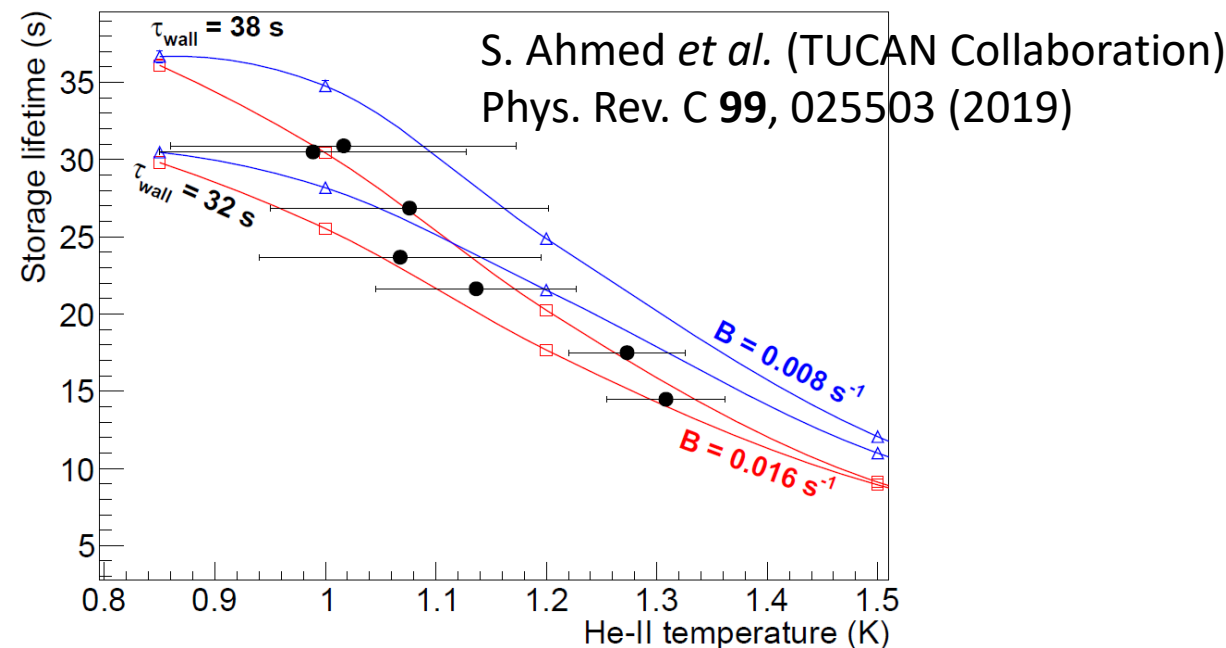
Structure of the TUCAN source (the “horizontal source”)



- Key issues:
 - Making as many 1 meV neutrons as possible. These neutrons have a large cross-section to downscatter to zero energy in superfluid helium.
 - Keeping the superfluid helium as cold as possible (losses $\sim BT^7$)



- Solutions:
 - Liquid deuterium cold moderator
 - High power helium-3 refrigerator directly coupled to the UCN production volume through UCN-compatible HEX, long horizontal channel of He-II.

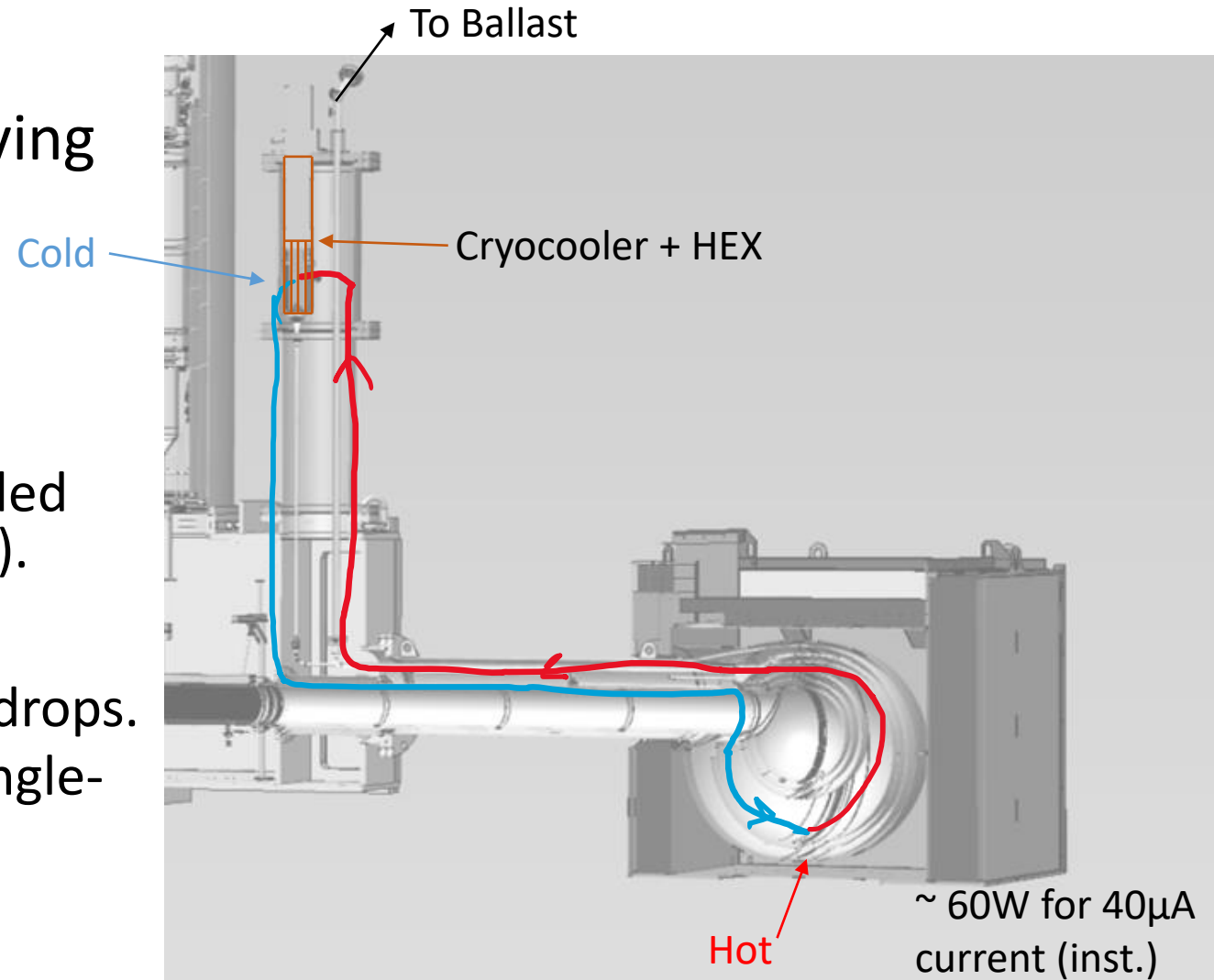


This presentation

- Two time-dependent 1D models of thermodynamic performance of two different parts of our UCN source:
 1. A liquid deuterium thermosyphon, delivering 60 W of cooling power (15 W time-averaged) to the LD2 cold neutron moderator.
 2. Heat transport through He-II in our prototype “vertical” source, and how this will be different after our upgrade to the “horizontal” source.

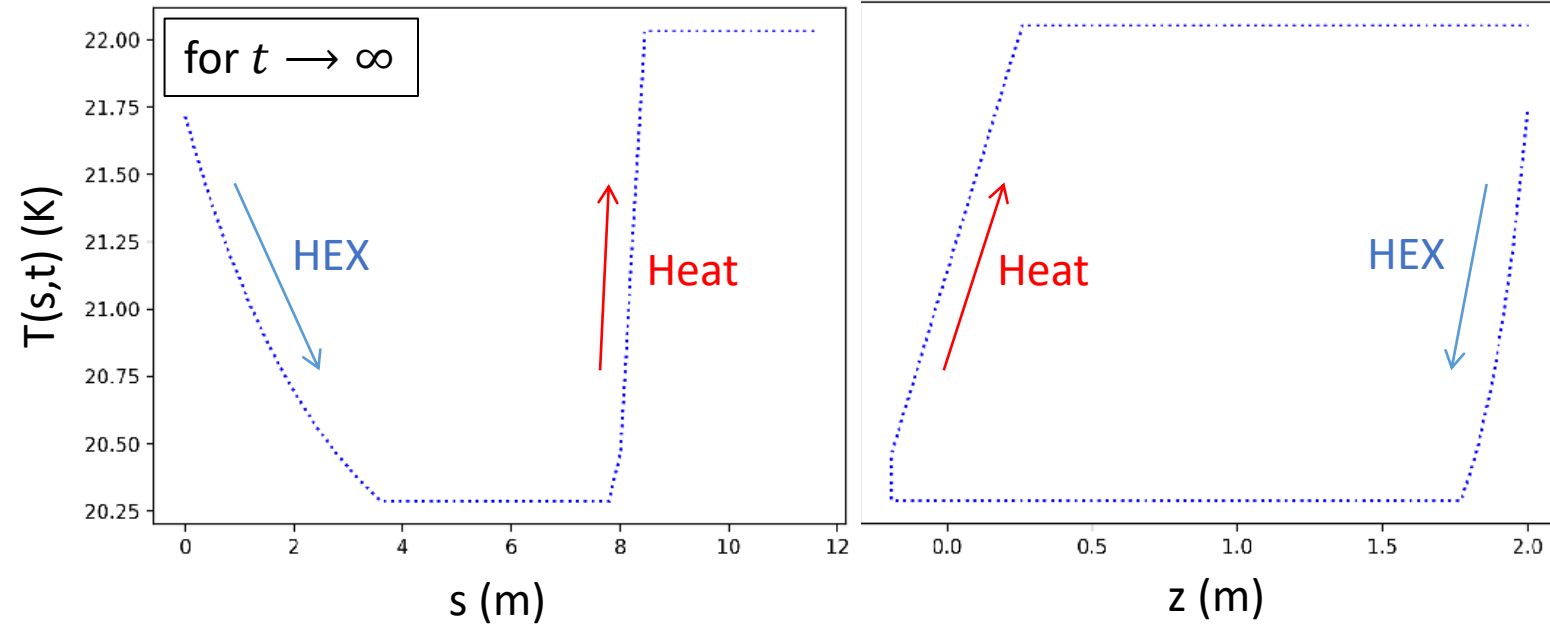
LD₂ thermosyphon (natural circulation system)

- Features: single-phase, no moving parts
- Studies by Kiera A.:
 - 1D time-dependent model of circulation.
 - HEX studies (fins vs. multi-threaded helix, heat xfer vs. pressure drop).
- Studies by Shawn S.:
 - Detailed accounting of pressure drops.
 - HEX study (1D correlations) of single-helix geometry



1D time-dependent model of circulation

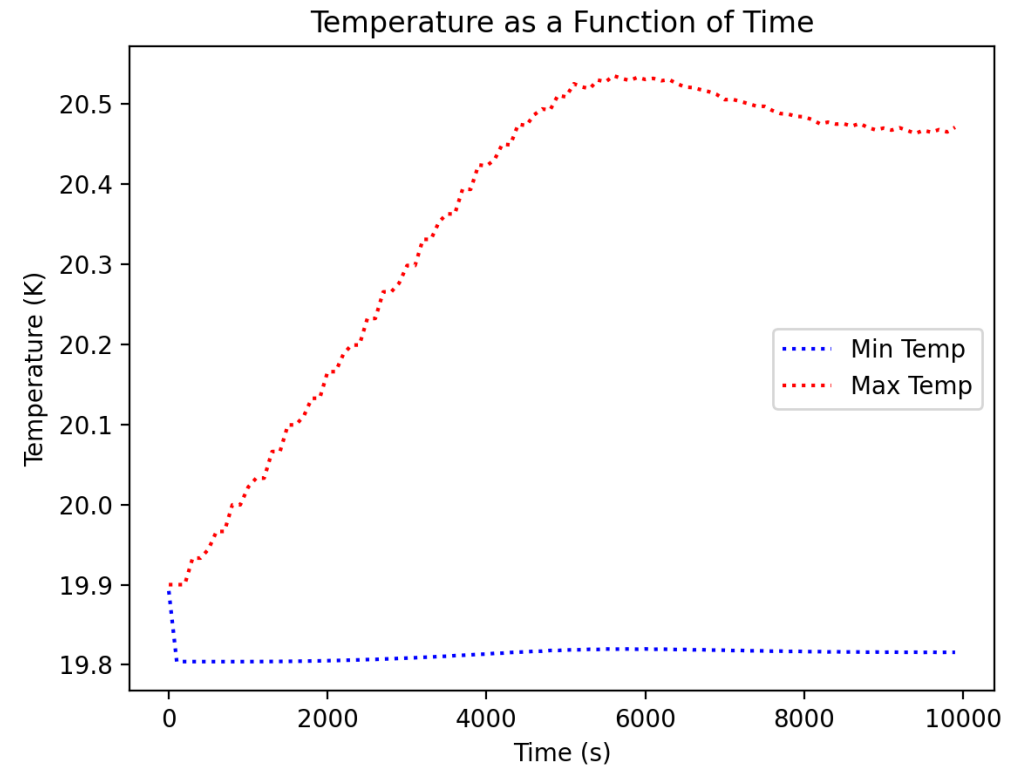
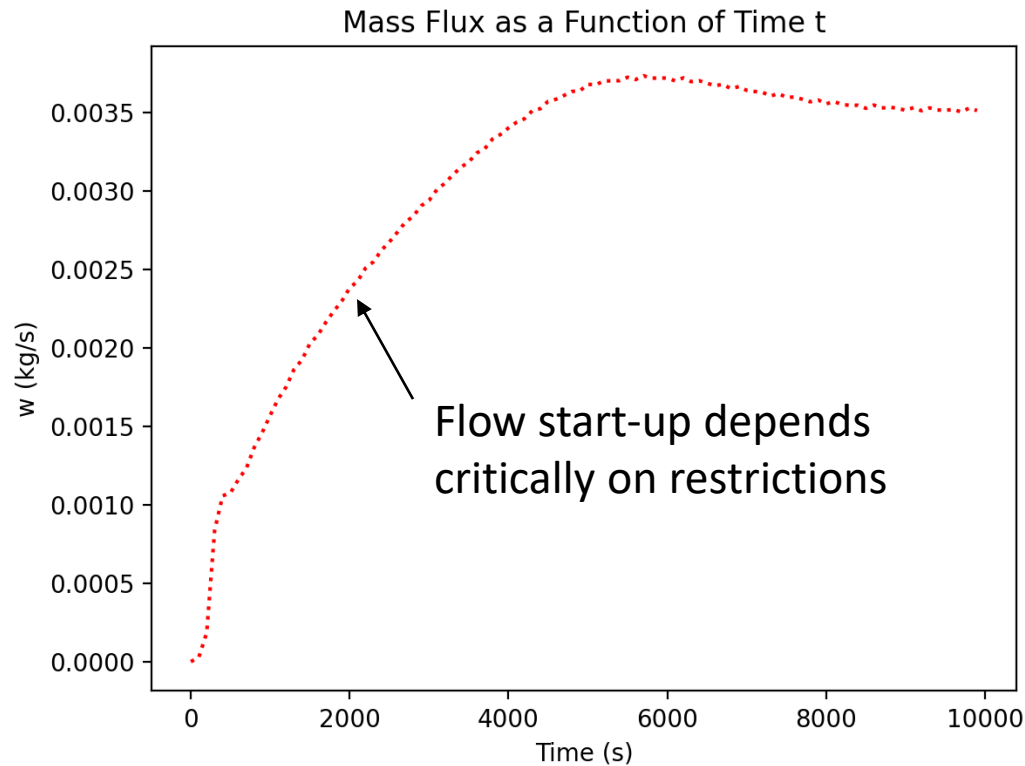
- Solve for
 - mass flow rate $w(t)$, and
 - temperature distribution $T(s,t)$ around the loop.



$$\frac{\partial T}{\partial t} + \frac{w}{A\rho_0} \frac{\partial T}{\partial s} = \begin{cases} \frac{Q}{V\rho_0 C_p} & \text{for } s \text{ in the heater} \\ 0 & \text{for } s \text{ in the connecting (insulated) pipes} \\ -\frac{4h_c(T-T_s)}{D\rho_0 C_p} & \text{for } s \text{ in the cooling heat exchanger} \end{cases}$$

$$\Gamma \frac{dw}{dt} + \frac{w^2}{2\rho_0} \sum_i \left(\frac{fL_{\text{eff}}}{DA^2} \right)_i + \rho_0 \beta g \oint T(s,t) dz = 0$$

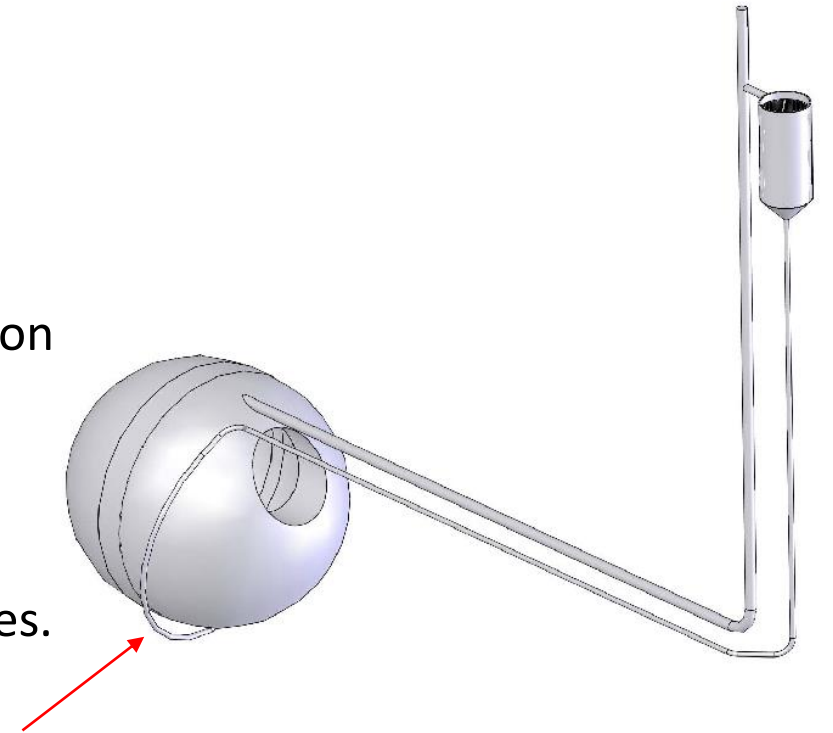
1D time-dependent model of circulation



- In these simulations, beam-pulsing is switched on with $\frac{1}{4}$ duty cycle, one minute on, three minutes off.
- Very similar results for CW beam at $\frac{1}{4}$ power.

1D circulation simulation status/results

- Simulation now includes:
 - Flow and temperature profile of liquid (as shown)
 - Heat transfer to walls, temperature profile of walls
 - Heat conduction (thermal diffusivity) in both LD₂ and walls
 - Ability to turn on/off beam at will
- A few key conclusions:
 - Flow response to heat is very slow. Initiating a flow depends on geometry. We will use a heater in low position to help this.
 - Regular beam pulsing doesn't affect flow, once flow has been established.
- To do (S. Stargardter):
 - Revise 1D time-dependent model with detailed pressure losses.
 - Special attention to heat deposited in the 2nd downcomer inside LD₂ bulb, to check that flow can be established



Time-dependence of He-II temperature

- A question often asked: what's better about your new UCN source?
- Partial answer: It can handle more power from beam heating. The He-II stays cold, even at considerably higher power.
- More informative answer: Compared to our old “vertical” source, the way heat is removed from the He-II in new “horizontal” source is completely different.
- In this work, we created a time-dependent model of heat transport in our He-II involving quantum turbulence (the Gorter-Mellink regime of heat transport)

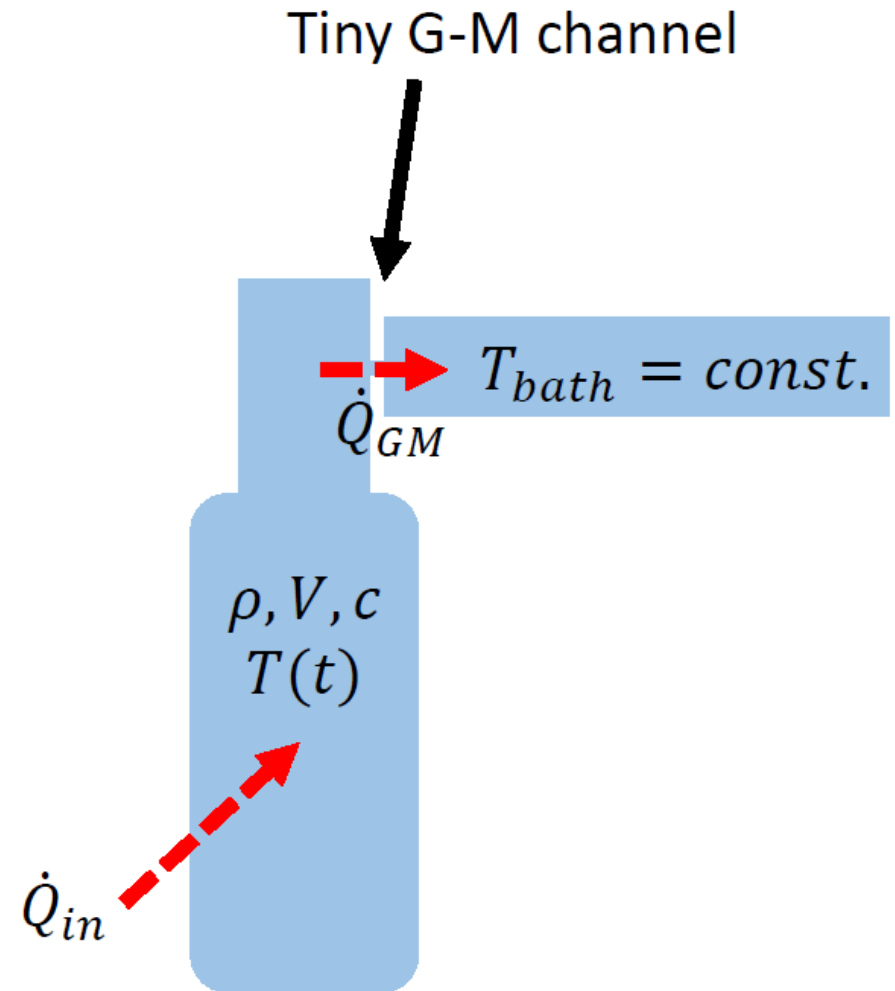
1D Model of He-II conduction, vertical source

$$\rho V c \frac{dT}{dt} = \dot{Q}_{\text{in}} - \dot{Q}_{\text{GM}}$$

$$dT/dx = -f(T, p)q^m$$

$$\rho V c \frac{dT}{dt} = \dot{Q}_{\text{in}} - A \left[\frac{1}{\ell} \int_{T_{\text{bath}}}^{T(t)} dT' f^{-1}(T', \text{SVP}) \right]^{1/m}$$

- Solve for $T(t)$
- Somewhat unknown:
 - A (area of the channel)
 - ℓ (length of the channel)
 - T_{bath} (He-II temperature close to HEX)
 - Background heat



Sample results, after some tweaking

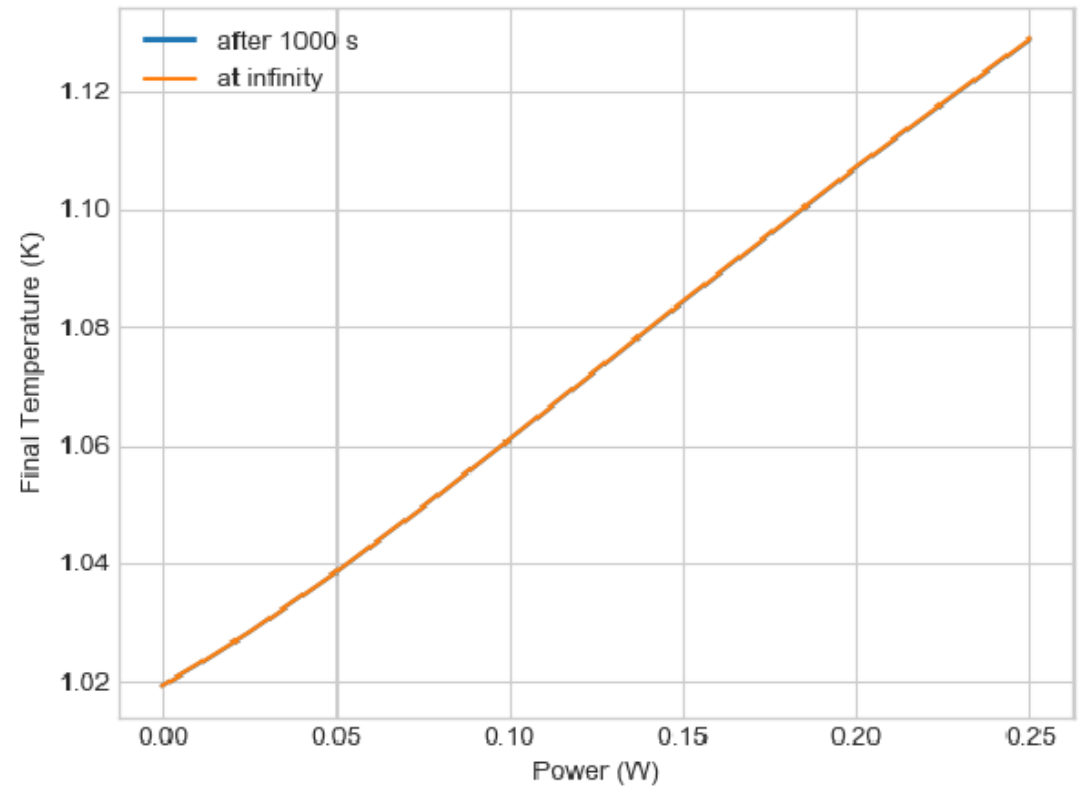
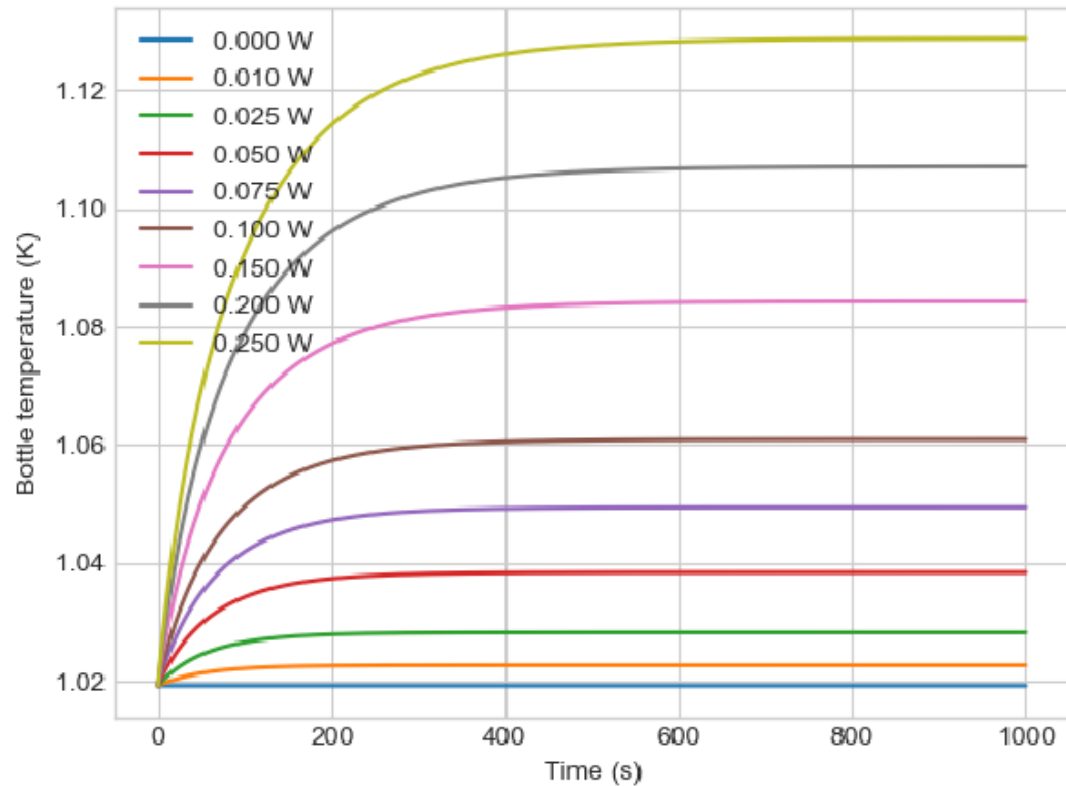
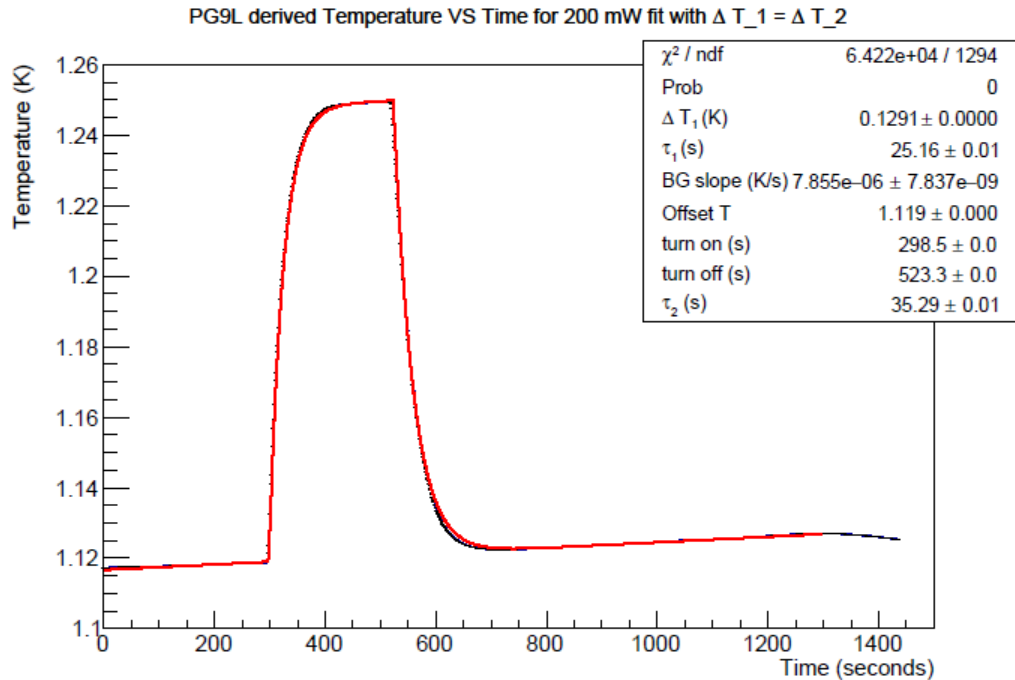


Figure 7: Left: time-dependence of temperatures for $\ell = \sqrt{A} = 0.01$ m with a background heat of 150 mW. Right: values at $t = \infty$ compared with final value from time-dependent calculation.

Comparison with Temperature data from vertical source (S. Hansen-Romu)



The Theory parameters that minimizes the fit to the data

Q_{BG} fixed	channel length, l (m)	T_{hex} (K)
0.20 W	0.0066	0.92
0.15 W	0.0062	1.07
0.10 W	0.0056	1.11
0.05 W	0.0051	1.12

- Simple 1D model gives good agreement with scale of heat flow restrictions, temperature rise, timescale, and background heat.

How is this different for the horizontal source?

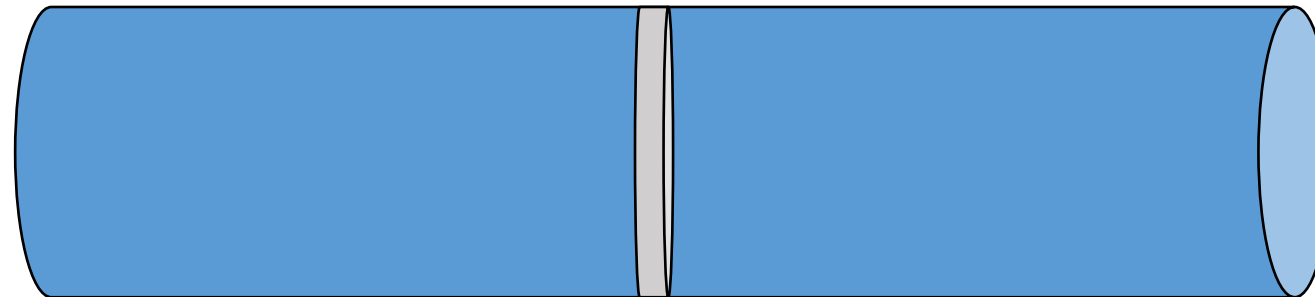
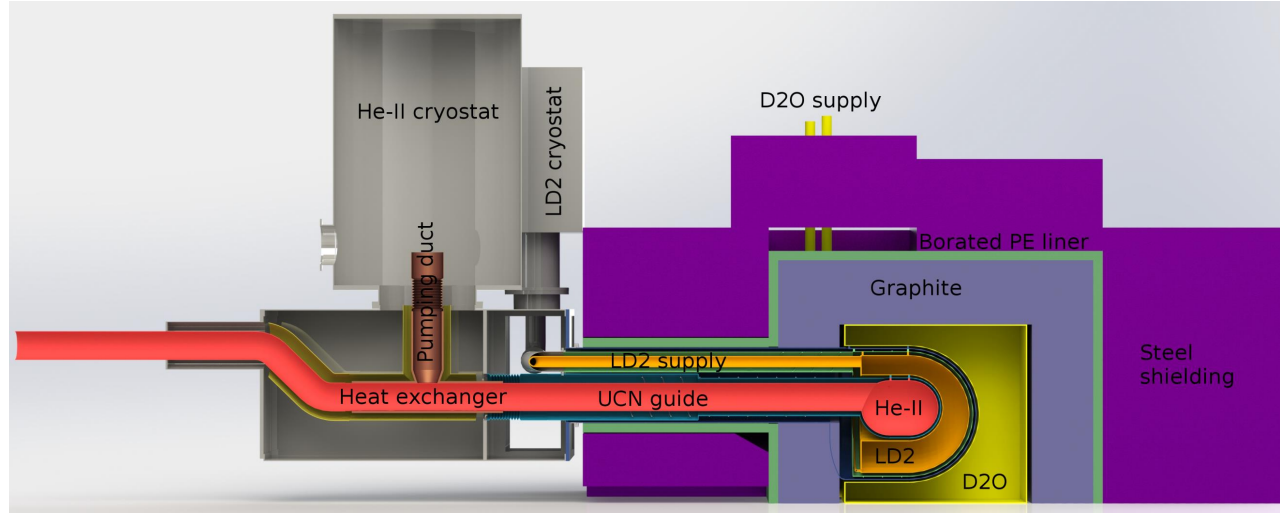
Conventional

$$q = k \frac{\partial T}{\partial x}$$

Gorter-Mellink

$$q^3 = f(T)^{-1} \frac{\partial T}{\partial x}$$

$$\frac{\partial T}{\partial t} = - \frac{1}{\rho c_p} \frac{\partial q}{\partial x}$$



$$T_o = 1.0K$$

$$\frac{q}{A} = 10^W/m^2$$

Conclusions

- Thermodynamics is useful to design particle physics experiments!
- 1D time-dependent model for LD₂
 - Gives time-dependence of thermosyphon start-up and beam pulsing.
 - Beam pulsing not a huge issue.
 - Start-up will be studied again to account for detailed pressure-drop model
- 1D time-dependent model for He-II
 - Model describes temperature rises and time constants in the vertical source rather well, with few “fit parameters”.
 - Comparing to the future horizontal source gives a more quantitative assessment of how the horizontal source will be superior, cryogenically.

Thank you!

Questions?